

1      Assessment of two different rapid compression tests for the evaluation  
2                      of texture differences in osmo-air-dried apple rings

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14  
15      **Abstract**

16              Mechanical properties of dried apples rings were studied through two different rapid compression tests. A  
17      bending-snapping test and a modified compression-relaxation test were performed in order to differentiate between  
18      osmo-air-dried apple rings as a function of variety (*Golden Delicious* and *Pink Lady*<sup>®</sup>) and drying temperature  
19      (70°C, 80°C, 90°C). Elastic modulus during bending, fracturability indices, peaks density, and relaxation coefficient  
20      during compression were taken into consideration. The obtained results reflect primarily the effect of the drying  
21      process on the moisture content of both varieties, but also the different changes in the tissues structure related to  
22      both the different solid-liquid exchanges during the osmotic pre-treatment and the drying process. Undergoing the  
23      same drying treatment, *Pink Lady*<sup>®</sup> rings showed a more rigid and stiff texture than *Golden Delicious*, which in  
24      contrast had a more brittle texture. The obtained results described satisfactorily structural changes of apple tissues,  
25      giving the possibility to discriminate, in a rapid way, between different categories of dried apples.

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29      *Keywords:* Apple rings; Drying; Texture; Compression test; Fracturability

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## Nomenclature

$b$	relative preponderance of low intensity vs. high intensity fractures	<i>Greek</i>	
$C$	number of fractures below a minimum observable non-zero stress reduction	$\varepsilon$	true deformation
$d$	diameter (mm)	$\sigma$	stress (kPa)
$E$	elastic modulus, slope (kNmm <sup>-2</sup> )	$\Delta x_i = x_i - x_{i-1}$	incremental changes in stress during compression
$F$	force (kN)	$\Delta L$	flexure between $X_H$ and $X_L$ (mm)
$F_c$	cumulative fracturability		
$L_V$	support separation (mm)	<i>Subscripts</i>	
$h$	height of sample (m)	$0$	initial
$R^2$	determination coefficient	$i$	inner
$S$	cross-section area perpendicular to force (mm <sup>2</sup> )	$o$	outer
$X_H$	end of $E$ -modulus determination (kN)	$r$	relative
$X_L$	beginning of $E$ -modulus determination (kN)	$\tau$	final
$y$	frequency		
$p$	probability value		
$P_d$	peaks density		

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## 34 1. Introduction

35 Apples are the fourth most important tree fruit crop worldwide after all citrus, grapes and banana. The world  
36 production of apples is more than 45 million tons (<http://www.fao.org/es/ess/top/commodity.html>). China is the  
37 world's largest apple producer (25.006.500 T), followed by the U.S. in second place (4.254.290 T); Turkey, Iran,  
38 Italy, France, Poland and Russian Federation produce each more than 2 million tons. Americans eat about 8.9 kg of  
39 fresh apples annually, compared to about 20.9 kg consumed annually by residents of European Countries. In  
40 addition to the primary consumption as fresh fruit, apples can be canned, juiced and fermented to produce apple  
41 juice, cider, vinegar, and pectin. Apples are an important ingredient in many desserts.

42 Recently new interest has arisen in the field of dehydrated apple products, used mainly as snack food ([Lewicki](#)  
43 [and Jakubczyk, 2004](#); [Velic et al., 2004](#)). However, air drying of vegetable tissues is characterized by extensive  
44 shrinkage and microstructural changes ([Aguilera and Stanley, 1999](#); [Bai et al., 2002](#)). This phenomenon affects the  
45 rate of drying as well as physical and functional properties of the dehydrated products. Maximal shrinkage during  
46 drying of a fruit material decreases as its solids increase and structural collapse was shown to decrease when fruit  
47 was impregnated with sugars prior to air drying ([Del Valle et al., 1998](#); [Lerici et al., 1985](#); [Riva et al., 2005](#);  
48 [Torreggiani, 1993](#)). Partial dehydration and solute intake can be achieved by immersion in concentrated aqueous  
49 solutions, the so called osmotic dehydration process ([Torreggiani and Bertolo, 2004](#)). By modifying the extent of the

50 partial dehydration and syrup composition not only can the end product be diversified but chemical, physical and  
51 functional properties can be improved. Both osmotic dehydration and air drying could produce great changes in the  
52 structure of vegetal tissue, as widely reviewed by Lewicki (Lewicki, 1998; Lewicki et al., 1997; Lewicki and  
53 Jakubczyk, 2004). In particular, texture of material moves from elastic-visco-plastic to rigid, becoming fragile and  
54 brittle. These changes are welcomed when they have to be transformed into a snack food such as apple chips, in  
55 which ‘crispy’ and ‘crunchy’ are sensory attributes greatly influencing quality evaluation by the consumers, as  
56 demonstrated by Shewfelt (1999).

57 The interest towards the production and preservation of crispy foods is also showed by the large number of  
58 published scientific research dealing with ‘crispy/crunchy’ attributes, as widely reviewed by Roudaut et al. (2002).  
59 Crispness and crunchiness are strongly linked to fracture and breaking characteristics of the product (Vincent, 1998).  
60 A crispy and crunchy product should indeed fracture and break into little pieces during biting and chewing as a  
61 consequence of a firm and brittle physical structure (Dijksterhuis et al., 2007). Different instrumental measurements  
62 were assessed to evaluate the texture of apples taking into consideration several attributes such as hardness,  
63 crispness, ripeness. Nevertheless, the obtained results are often hard to compare, hence not of general use (Marquina  
64 et al., 2001), due to their high dependency from a lot of factors such as cultivar, process conditions, specific drying  
65 process method, and presence or absence of pre-treatment (Ratti, 1994; Sjöholm and Gekas, 1995). For that reason,  
66 the parameters taken into account were often interpreted in different ways. So, according to Harker et al. (2003), it is  
67 necessary to compare specific categories, to strengthen the link between product and quality in the consumer’s  
68 perception. To this purpose, instrumental tests should be accurately performed in accordance with the specific  
69 instance (Marquina et al., 2001).

70 The aim of this work was to set two different rapid compression tests in order to obtain parameters to use as  
71 indices of textural characteristics of osmo-air-dried apple rings obtained using two different cultivars and three  
72 different drying temperatures.

73

## 74 **2. Materials and Methods**

### 75 *2.1 Apples*

76 Two cultivars of organic apples were used: Golden Delicious and Pink Lady®, both cultivated in the Research  
77 Centre for Agriculture and Forestry (Laimburg, BZ, Italy). Apples, harvested at the same maturity stage (Golden

78 Delicious: dry matter 14.84%, acidity 10.73 meqNaOH/100 g, refractive index 13.05 °Bx; Pink Lady®: dry matter  
79 15.96%, acidity 9.70 meqNaOH/100 g, refractive index 14.10 °Bx), were washed, dried and cored by a spoon soil  
80 auger (25.0 mm diameter). Finally, they were mechanically cut (LT INOX, Kronen, Germany) into 5.0 mm thick  
81 rings.

82

## 83 2.2. *Treatments*

### 84 2.2.1. *Osmotic dehydration*

85 Apple rings were dipped for 60 minutes at 25°C in a maltose solution (Sirtori et al., 2007) ( $a_w = 0.90$ ; 62.8 %  
86  $w/w$ ), which was continuously recirculated through a peristaltic pump. The ratio fruit/solution was 1/3.

87 Soluble solids gain (SG) and water loss (WL) were calculated according to Giangiacoimo et al. (1987), and are  
88 expressed as g/100 g of initial fresh fruit weight.

89

### 90 2.2.2. *Air drying*

91 Air drying was performed at 70°, 80° and 90°C, up to a constant weight, using a pilot alternate upward-  
92 downward air circulated drier (Thermolab, Codogno, Italy) operating at an air speed of 1.5 m/s. For all samples, the  
93 equilibrium weight (i.e. the constant weight) was achieved when the difference in weight was less than 1 mg/g solids  
94 after 90 additional minutes of drying.

95

## 96 2.3. *Chemical analyses*

97 Raw apple dry matter and total titratable acidity were determined according to AOAC methods (1985);  
98 refractive index (°Bx) using a Multiscale automatic refractometer (mod. RFM91, BS, UK).

99 Osmo-air-dried apple rings water activity ( $a_w$ ) was measured by an electronic hygrometer (Aqua Lab. CX-2 –  
100 Decagon Devices, Pullman, USA), based on the determination of the dew point and previously calibrated with a  
101 standard solution of LiCl of known activity (prepared by High-Purity Standards for Decagon Devices). Results are  
102 the mean of 6 determinations. Moisture content was determined according to Karl Fischer method after extraction in  
103 anhydrous methanol (ASTM D 6304-2004 a, 1-procedure A). Results are the mean of 3 determinations and are  
104 expressed as g H<sub>2</sub>O/100 g solids.

105

106 2.4. Mechanical analyses

107 2.4.1. Stress-Relaxation test (modified)

108 A  $40 \pm 2.0$  mm pile of apple slices one upon the other was put into a steel cylinder placed between a lower (150  
109 mm diameter) and an upper plate (80 mm diameter). The latter was connected with a Zwick Machine (mod. Z005,  
110 Zwick Roell, Germany) fitted with a 100 N load cell. Apple slices were compressed by the upper plate at a speed of  
111 10 mm/min. This slow speed was set to allow a better observation of each compression step rather than at higher  
112 speed, in order to carry out the next quantification of fracturability. At 20% deformation, the crosshead surface was  
113 stopped and the pile was allowed to relax for 20 s, which is a shorter time than a typical compression-relaxation test.  
114 The relaxation time selected in this work is due to the fact that stiff material is able to accumulate stress and to relax  
115 fast and brittle material shows a very small relaxation because most of stress accumulated during compression is  
116 consumed in the breaking work. Hence, apple rings analyzed in this work were able to relax within 20 s (i.e. the  
117 specified interval of time for relaxation) at least 70% of the total stress developed during compression. Therefore,  
118 the obtained curves will show only two of the three typical zones described by [Bhattacharya and Narasimha \(1997\)](#):  
119 the first characterized by a sharp decrease of the stress and the second showing a reduction of the rate of decrease.  
120 Both the stress-strain and the stress-time profile were continuously recorded and the following parameters were  
121 calculated directly by the software (TestXpert V10.11 Master):

122

- 123 • *True deformation:*

124 
$$\varepsilon = -\ln\left(1 - \frac{h_0 - h_\tau}{h_0}\right) \quad (1)$$

- 125 • *Stress:*

126 
$$\sigma = \frac{F}{S} \quad (2)$$

127

- 128 • *Relative relaxation stress:*

129 
$$\sigma_r = \frac{\sigma_\tau}{\sigma_0} \quad (3)$$

130 Relative relaxation stress represents a part of the total stress that the material accumulated during compression and is  
131 not relaxed after a given relaxation time (Lewicki and Jakubczyk, 2004). Furthermore, according to the method for  
132 quantifying fracturability by Barrett et al. (1994), the distribution of fracture intensities occurring during  
133 compression in the 4-20% strain region was quantitatively described through the following exponential function:

134

$$135 \quad y = Ce^{(b\Delta_{xi})} \quad (4)$$

136

137 Decreases in stress (i.e. fractures) are given by negative  $\Delta_{xi}$  values; in contrast, positive values involve increases in  
138 stress due to compression. Only negative  $\Delta_{xi}$  values were taken into consideration to obtain the frequency  
139 distribution of fracture intensity. Parameters derived from the equation (4),  $C$  and  $b$ , were used as fracturability  
140 indices. Cumulative fracturability ( $Fc$ ) was used as further index. It was obtained by summing the fracture intensity  
141 of frequencies of each distribution. Finally, the density of peaks,  $Pd$  (number of peaks / deformation in mm) was  
142 used as a measure of brittleness of apple rings in the investigated region (4-20% strain).

143 All measurements were carried out on 10 different apple piles for each temperature condition and for each cultivar.

144

#### 145 *2.4.2. Bending-Snapping test*

146 Tests were carried out using a Zwick Machine (mod. Z005, Zwick Roell, Germany) fitted with a 100 N load  
147 cell. Slices were  $72.0 \pm 2.0$  mm in diameter and  $3.5 \pm 0.3$  mm thick after drying. So, the length of the specimen was  
148 at least 16.2 times greater than thickness, to avoid shearing and compression effects, compromising the final results  
149 (Bourne, 2002). In addition, to limit negative effects by shape and surface imperfections, discs as flat and regular as  
150 possible were selected. One apple disc at a time was placed on two supports separated by a distance of 45.0 mm,  
151 each one equipped with a 8.0 mm diameter horizontal rod at the tip. A third compressing bar, also a 8.0 mm  
152 diameter horizontal rod at the tip, was driven down between the two supports at a speed of 10 mm/min, bending  
153 each specimen until it snapped. The slope (i.e. the elastic modulus,  $E$ ) before the first fracturability peak of highest  
154 magnitude was calculated from the force-displacement curves as the index of crispness (Jackson et al., 1996;  
155 Konopacka et al., 2002) of the dried apple rings, in accordance with the following equation which takes into  
156 consideration the actual surface area of the rings in contact with the upper bar (i.e. without the central part of 25.0  
157 mm diameter):

158

$$E = \frac{[8 \times Lv^3 \times (XH - XL)]}{[6 \times \Delta L \times \pi \times (d_o^4 - d_i^4)]} \quad (\text{kNmm}^{-2}) \quad (5)$$

160

161 Ten replicates for each air temperature and for each cultivar condition were made.

162

### 163 2.5. Statistical analysis

164 The effect of temperature conditions and cultivar was statistically assessed using a two-way analysis of  
165 variance. The mean values, when appropriate, were compared by LSD (least significant difference) multiple range  
166 test at  $p \leq 0.05$  (or 95% confidence interval) using Statgraphics Plus 4.0 software (STSC Inc, Rockville, USA).  
167 Intensity distributions were fitted by an exponential model with two constants using a nonlinear curve-fitting  
168 package (Tablecurve 4.0, Jandel Scientific, San Rafael, USA).

169

## 170 3. Results and discussion

### 171 3.1. Stress-Relaxation test

172 The three different curves (each one as a mean of ten replicates) resulting from the compression-relaxation test  
173 of the Golden Delicious cultivar reported in Fig. 1 show the effect of air temperature on the relaxation characteristics  
174 of apple rings. The curve profile (similar for the three lots) is characterized by three observable parts: an initial  
175 rising tract, culminating in a first fracture, that represents the deformability prior to rupture of the structure; a  
176 halfway jagged-oscillating zone, depending on the brittleness of the samples, indicating the deformation and  
177 destruction of internal structure; a final descending smooth tract (after about the first 2/3 of each curve), along which  
178 part of the stress accumulated during compression is relaxed. This shape is typical for foods characterized by a  
179 crunchy or crispy texture, like breakfast cereals and snacks. Relative relaxation stress values ( $\sigma_r$ ) (Table 1) indicate  
180 that the three different drying temperatures were able to produce significant effects on apple rings. In fact, after a  
181 relaxation time of 20 s, the amount of not relaxed stress increased from about 65% (70°C) to almost 90% (90°C).  
182 Moreover, a significant difference was observed between the two varieties. In particular, the number of cavities and  
183 voids formed by drying could play an important role in defining the compression-relaxation curves (Lewicki and  
184 Jakubczyk, 2004). These changes are strongly related to the tight relationship between temperature and moisture

185 content in the biopolymer matrices, as can be seen in [Table 1](#). Moisture content of osmo-air-dried apple rings  
186 decreased for both varieties as the drying temperature increased (60% approximately from 70°C to 90°C). At all the  
187 tested temperatures, Pink Lady® osmo-air-dried rings had a significantly lower moisture content than the Golden  
188 Delicious ones, probably due to intrinsic factors (e.g. composition, cellular shape and tissue structure), together with  
189 the diverse solid-liquid exchanges during the osmotic pre-treatment. Soluble solid gain and water loss were 4.913  
190 and 11.013, respectively for Golden Delicious, and 3.651 and 6.903 respectively for Pink Lady®, leading to a dry  
191 matter content of 21.358 for Golden Delicious and 21.192 for Pink Lady®. As a consequence of the decrease in  
192 moisture content,  $a_w$  decreased moving from 70°C to 90°C for both cultivar, even if a statistical significant  
193 difference was assessed only within but not between each group (i.e. variety).

194 Considering that the higher the drying temperature the lower the moisture content and water activity values, the  
195 different trend of the curves reported in [Fig. 1](#) can be better interpreted. At 70°C the material maintained fairly  
196 elastic-plastic behaviour (as shown by the smooth ascent part of the curve) and it relaxes approximately 35% of the  
197 developed stress. As temperature increased, the texture profile of apple rings changed, as confirmed by the  
198 ruggedness of the curves. As ascertained by several researchers, these results are related to the removal of water  
199 during drying. In fact, the convective flux of hot air yielded an almost total loss of the plasticizing effect of water,  
200 affecting the rheological properties of apple tissues and promoting some main physical phenomena (e.g. shrinkage,  
201 moisture gradients) especially in the first step of drying ([Lewicki and Lukaszuk, 2000](#)).

202 The overall relationship between moisture content, water activity and relative relaxation stress is shown in [Fig.](#)  
203 [2](#). Moving from 70°C to 90°C both water activity and moisture content decreased drastically, causing an increase of  
204 relative relaxation stress as a consequence of rigidity gained by apple tissues, which are unable to relax most of the  
205 induced stress. Indeed, the majority of the stress developed during the compression phase is relaxed abruptly by  
206 simultaneous failures. At any of the drying temperatures moisture content and water activity values of Pink Lady®  
207 rings were lower than those of Golden Delicious, whereas RRS values were significantly higher. These results  
208 evidenced that the original structure and composition, together with the different solid-liquid exchanges during the  
209 osmotic pre-treatment could play an important role in determining the extent of heat-induced micro-structural  
210 modification, such as cell separation, cellular collapse and, in general, damage to cell walls and membranes.

211

212 *3.2. Fractures quantification*

213 A further measure of the brittleness of apple rings is the degree of jaggedness of their stress-strain curve. It can  
214 be assessed in different ways, for example, by the power spectrum of the Fast Fourier Transform and the Natural  
215 Fractal dimension of normalized compression curves (Peleg, 1997). In the present study, the distribution of fracture  
216 intensities occurring during the first step of compression-relaxation test was quantitatively described by an  
217 exponential function. By using mathematical procedures ‘easy-to-use’ by the common statistical programs, main  
218 parameters used as fracturability indices were obtained. In a first step, a frequency distribution of changes in stress  
219 during compression was constructed as described by Barrett et al. (1994) for each air temperature condition and for  
220 both varieties (Fig. 3 a, b, c). Here, descent negative lines indicate fractures, whereas positive tracts are for  
221 increases in stress due to compression. Moving from the lowest to the highest temperatures, graphs result in more  
222 evident noise due to an increase of fractures and ruptures of specimen. Furthermore, a substantial difference exists  
223 between the two varieties: for each drying temperature, Golden Delicious graphs show the greatest number of  
224 failures over the whole strain path, whereas Pink Lady® led to graphs with the longest negative lines (i.e. the greatest  
225 fracture intensities).

226 In a second phase, each average intensity distribution was fitted to the Eq. (4) and coefficient  $C$  and  $b$  were  
227 calculated to be used as fracturability indices. Fracture intensity distributions for both varieties are presented in Fig.  
228 4, whereas the corresponding  $b$  and  $C$  indices are reported in Table 1. At each temperature the highest number of  
229 breaks (high frequency values) corresponds to the lowest fracture intensity values (on the right of the x-axis) for  
230 both apple varieties. Still, a significant difference is observed between the two varieties. At 70°C and 80°C the  
231 number of low intensity fractures was higher for Pink Lady® (45 and 109 frequencies, respectively) than for Golden  
232 Delicious (17 and 74 frequencies, respectively). At 90°C, the low intensity fractures number for Golden Delicious  
233 was about twice as high (241, as a sum of the two values around -0.1 kPa indicated by the letter A and B in Fig. 4)  
234 as Pink Lady® (122, indicated by the C letter in Fig. 4). The latter showed a higher number of high intensity  
235 fractures, i.e. a larger number of data points at the highest negative values of stress, corresponding to the largest  
236 fracture intensities. These results were confirmed by the  $b$  and  $C$  coefficients, highlighting the effect of drying  
237 temperature on moisture content. High values of  $b$  were calculated for Pink Lady® only at 70°C and 80°C (61.288  
238 and 14.003, respectively, vs. 60.711 and 9.279 for Golden Delicious). At the highest temperature (90°C) the two  
239 cultivars behaved in an opposite way, in that the highest value of  $b$  index was for Golden Delicious (4.724) rather  
240 than for Pink Lady® (3.328). With respect to  $C$  coefficient, Pink Lady® rings yielded the highest values at 70°C and

241 80°C air temperature, whereas at 90°C the maximum was for Golden Delicious. This means that the number of  
242 fractures below a minimum observable non-zero stress reduction is greater for Golden Delicious only at the highest  
243 drying temperature. This is in agreement with the  $F_c$  index, as reported in [Table 1](#). In fact, values of this coefficient  
244 confirmed that the total number of breaks was greater for Pink Lady® (58 vs. 29) at 70°C and for Golden Delicious  
245 (360 vs. 265) at 90°C. Nevertheless, in contrast to  $C$  index values at 80°C, the total number of failures were higher  
246 for Golden Delicious (166 vs. 135) at this drying temperature.

247 The last criteria considered to measure the extent of fracturability of differently dried apple rings is the peaks  
248 density,  $Pd$ . As shown in [Table 1](#), this index was determined considering peaks of magnitude both equal and greater  
249 than 0.5% and 5.0% the maximum force (i.e. the highest peak) registered during compression. In the first case  
250 (peaks  $\geq 0.5\%$  maximum force) ruptures of small and large intensity were simultaneously measured, whereas in the  
251 second (peaks  $\geq 5.0\%$  maximum force) only the largest ones were taken into consideration. Both at 0.5% and 5.0%,  
252 and also for both varieties, this index increased along with drying temperature, though a difference was observed  
253 between Golden Delicious and Pink Lady®, mainly at 80°C and 90°C. For peaks  $\geq 0.5\%$  the maximum force, the  
254 Golden Delicious had  $Pd$  values greater (80°C) and fairly similar (90°C) to those of Pink Lady®. In contrast, for  
255 peaks  $\geq 5.0\%$  the maximum force (i.e. only peaks of large intensity), Pink Lady® had the highest  $Pd$  values both at  
256 80°C and 90°C. This behaviour indicates that during compression Golden Delicious originated fractures to a smaller  
257 extent than Pink Lady® at 80° and 90°C. On the contrary, Pink Lady® evidenced abrupt breaks during compression,  
258 causing ruptures of higher intensity. At 70°C, the density of peaks during the deformation range 4-20% was always  
259 greater for Pink Lady®, implying that when Golden Delicious rings are dried at this temperature they still keep their  
260 visco-elastic properties, whereas Pink Lady® rings start to acquire a more brittle texture.

261 Once again, the results relating to fractures quantification highlighted the significant difference between the two  
262 cultivars. After the same drying treatment, Pink Lady® rings acquire a stiffer and more rigid texture than Golden  
263 Delicious, which appear, in contrast, more brittle. From a practical point of view this fact may be important because  
264 Golden Delicious could be able to produce a more appreciable crispness and crunchiness sensation than Pink Lady®.  
265 This different behaviour can be attributed to the different impact of the drying treatment on the moisture content of  
266 the two different matrices as well as to the specific intrinsic characteristics of apple tissues. Furthermore, Pink  
267 Lady® apple rings have lower solid-liquid exchanges than Golden Delicious ones, therefore during drying their  
268 structure could be less protected from shrinkage ([Riva et al., 2005](#)). A further factor affecting the different behaviour

269 between the two cultivars is their firmness, due to the ripening stage. Even though Pink Lady® and Golden Delicious  
270 were used at the same maturity stage, it is known from the horticulture practice that Pink Lady cultivar loses its  
271 firmness slower than Golden Delicious. That would explain why Golden Delicious tissues are characterized by a  
272 lower strength (before and after drying) and also responded differently to osmotic treatment.

273

### 274 3.3. *Bending-Snapping test*

275 Fig. 5 and Fig. 6 show typical deformation curves obtained applying the bending-snapping test to Pink Lady®  
276 and Golden Delicious osmo-air-dried rings, respectively. The shape of each curve is strictly related to the specific  
277 temperature of the drying process, and thus to moisture content and water activity values. At 70°C, the curves show  
278 an initial rising tract, characterized by an almost linear relationship between force and deformation. After  
279 approximately 1.8 mm deformation, a first inflection of the curve indicates that this relationship becomes non-  
280 proportional. At 80°C the obtained curves show a profile similar to the 70°C curves during the initial displacement-  
281 path. However, after the first steep linear tract, the curve brakes abruptly, lacking the final descending part. This  
282 behaviour is more evident in the sharp curves obtained from apple rings dried at 90°C. In this case, the initial quick,  
283 steep and linear tract is immediately (after about 0.5 mm deformation) followed by two subsequent spiky peaks,  
284 relating to violent ruptures. As mentioned previously, the steepness of the slope at the beginning of each curve is  
285 defined as crispness (Jackson et al., 1996; Konopacka et al., 2002) and it is involved in the resistance of the  
286 specimen to bending. In accordance with the results reported in Table 1, a decrease in moisture content, as a result of  
287 each drying treatment, leads to increases in crispness. Curves derived from apple rings dried at 70°C had the lowest  
288 crispness coefficient, approximately 1.6 times (Pink Lady®) and 2 times (Golden Delicious) less than those obtained  
289 at 80°C. Drying at 90°C yields apple rings with the highest crispness values (50% and 30% more than those  
290 observed in Pink Lady® and Golden Delicious rings dried at 80°C, respectively), as evidenced by the steepest slope  
291 of the initial linear line of the curve. Drying temperatures of 90°C produced the crispiest dried apple rings, having a  
292 greater resistance to bending (Jackson et al., 1996). A statistically significant difference between apple varieties was  
293 observed. For all temperature-settings, Pink Lady® showed the highest crispness values, acquiring more stiffness and  
294 resistance to deformation than Golden Delicious, in accordance with moisture content values (higher for Golden  
295 Delicious), as shown in Table 1.

296 As shown in Fig. 2, the relationship between water activity and moisture content and crispness is inversely  
297 proportional: crispness increased as  $a_w$  and moisture content decreased. The effect of water can also be highlighted  
298 by the shape of the curves obtained at different temperatures. In general, the left-shifted bell-shaped curves obtained  
299 at 70°C (i.e. at the highest  $a_w$  and moisture content) were wide and smooth, reflecting the plasticizing effect of the  
300 remaining water. Moreover, the area under the curve was large (data not shown), indicating that a fair amount of  
301 energy is needed to promote the final failure of the specimen. At 80°C the obtained curves showed the increasing  
302 effect of drying temperature. The gain of crispness/crunchiness is also manifested in a more jagged relationship,  
303 indicating failures and ruptures, due to changes in the structure with the formation, for example, of cavities, voids  
304 and local damage (Lewicki and Jakubczyk, 2004). Finally, at 90°C (i.e. at the lowest  $a_w$  and moisture content), apple  
305 slices broke abruptly, like a brittle and fragile body. Furthermore, the area under the curve was small (data not  
306 shown), reflecting the low quantity of energy required to break the dried rings.

307 All the obtained results indicate that by increasing air temperature, the rheological characteristics strongly  
308 change for both variety, but differently. While Golden Delicious acquires rigidity but remains brittle and fragile (and  
309 hence develops small fractures in comparison to the other cultivar), Pink Lady® becomes rigid, but harder and  
310 stiffer, with abrupt failures of major intensity. It can be inferred that, besides chemical composition and moisture  
311 content, an important role may be played by the extent of dried apple rings porosity. This parameter in its turn is  
312 strictly linked both to intrinsic tissue characteristics of the cultivar and to the effect on the dried apple structure of  
313 the different soluble solids enrichment and water loss achieved through the osmotic pre-treatment. After drying,  
314 Golden Delicious may acquire an internal structure characterized by a greater number of cavities and voids than  
315 Pink Lady® that lead to a major brittleness during compression.

316

#### 317 4. Conclusions

318 Through the two different compression tests used in the present work numerical indices were obtained able to  
319 discriminate between two different cultivars osmo-air-dried at three different temperatures. The modified  
320 compression-relaxation stress test quickly supplied five parameters that can be used as fracturability indices,  
321 reflecting the brittleness of each specimen in terms of the degree of jaggedness of the stress-strain curve. The  
322 bending-snapping test provided a significant index able to discriminate between apples characterized by a different  
323 crispness. The ease and the speed of the described methods and the possibility to apply them using conventional

324 statistical software in a timely fashion, make the approach of this research a helpful tool to discriminate between  
325 different batches in the scale-up manufacturing of dried apple rings with specific textural characteristics.  
326 Furthermore, the applied methodologies appear suitable to be correlated with sensory evaluations concerning texture  
327 perception arising from trained panellists, in order to pinpoint the critical crispness values (i.e. the texture  
328 acceptance limits).

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453 **Figure captions**

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**Figure 1.** Typical compression-relaxation curves of osmo-air-dried apple rings piles (Golden Delicious): effect of drying temperature.

**Figure 2.** Relationship between moisture content, water activity, relative relaxation stress and crispness of apple rings osmo-air-dried to a constant weight at different temperatures.

**Figure 3.** Frequency distribution of stress intensities during compression of apple rings osmo-air-dried to a constant weight at 70°C (a), 80°C (b) and 90°C (c): Golden Delicious (left) and Pink Lady® (right). Each graph is the mean of ten replicates.

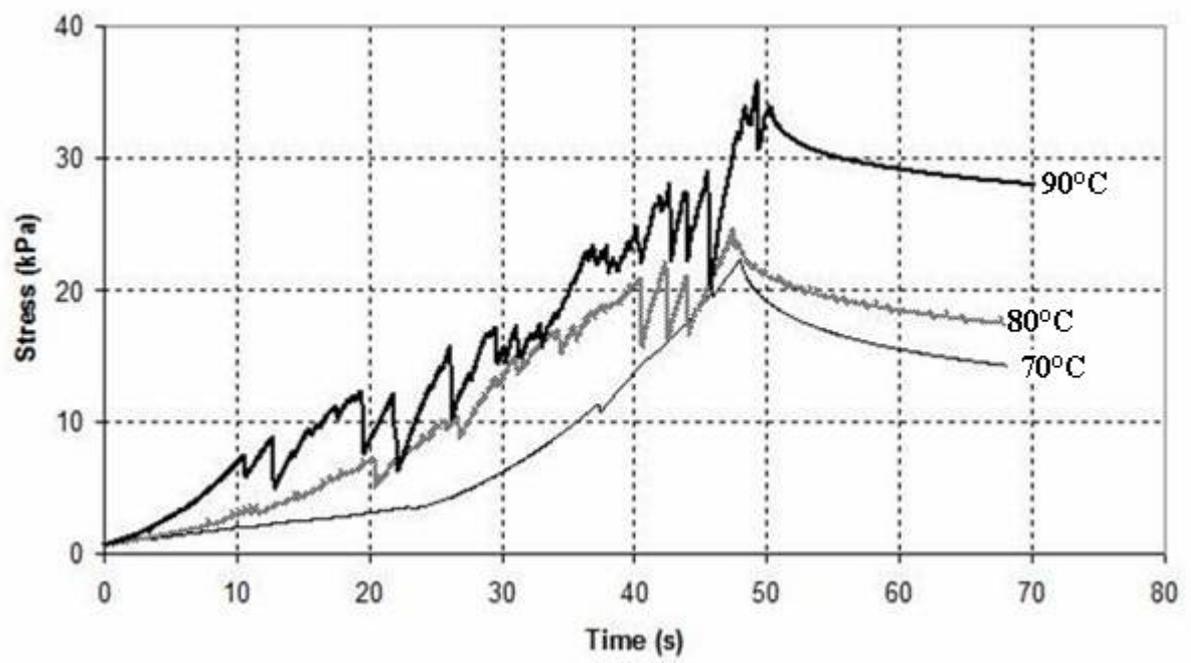
**Figure 4.** Fracture intensity distributions in apple rings osmo-air-dried to a constant weight at different temperatures: Golden Delicious (up) and Pink Lady® (down). Each graph is the mean of ten replicates.

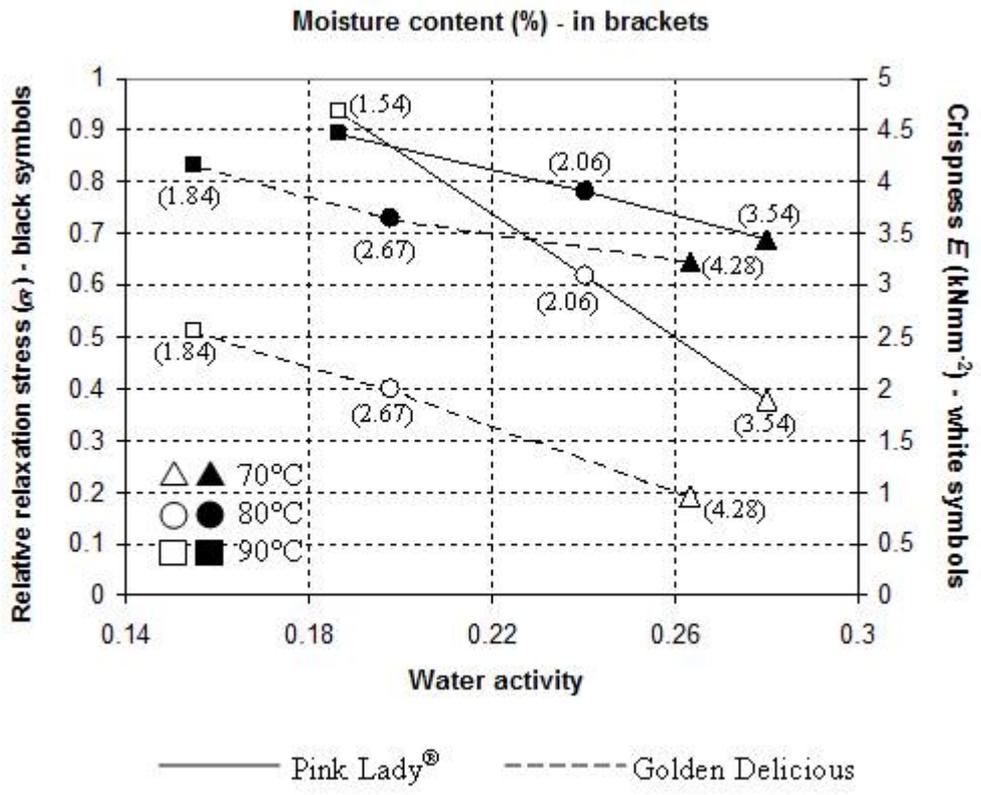
**Figure 5.** Force-deformation curve of apple rings (Pink Lady®) osmo-air-dried to a constant weight at different temperatures. The initial slope of each curve is evidenced inside the circle.

**Figure 6.** Force-deformation curve of apple rings (Golden Delicious) osmo-air-dried to a constant weight at different temperatures.

**Table caption**

**Table 1.** Characteristics of apple rings osmo-air-dried to a constant weight at different temperatures.





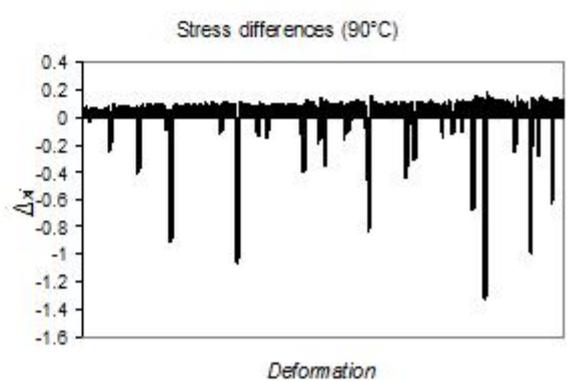
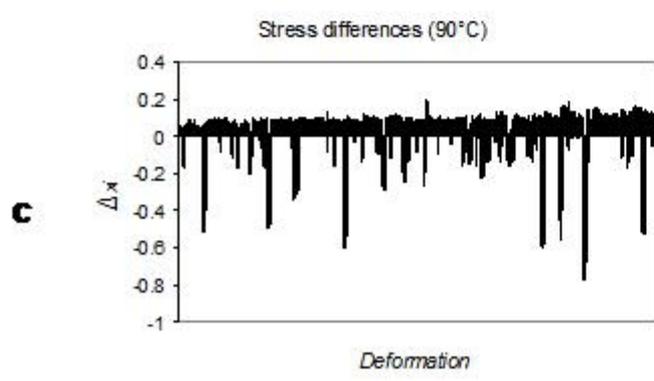
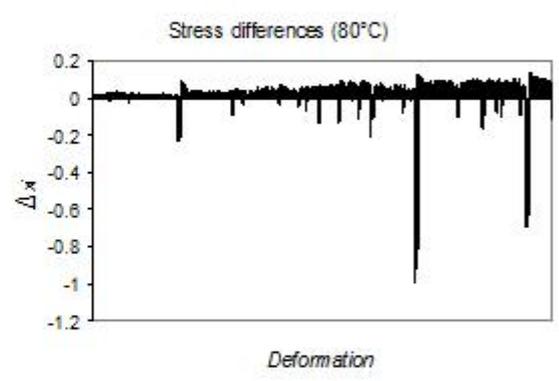
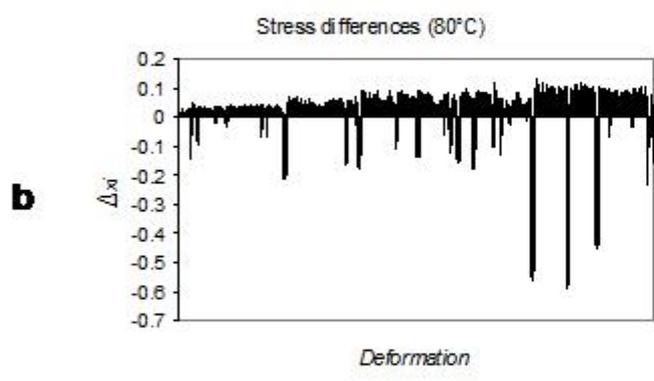
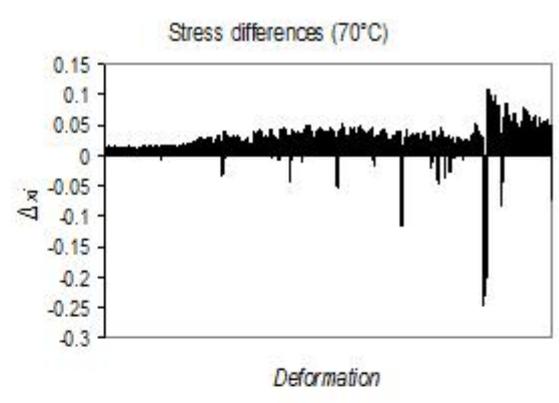
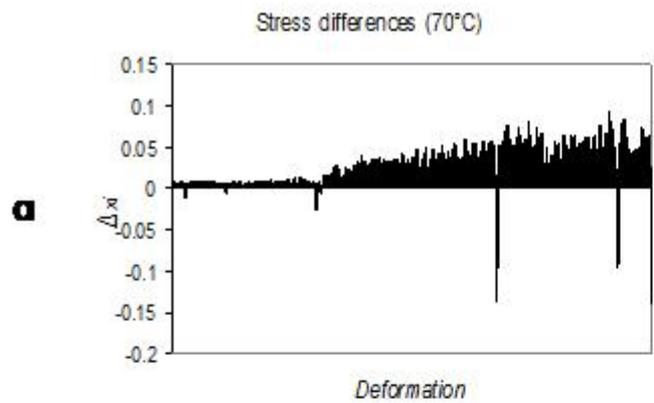


Figure 4

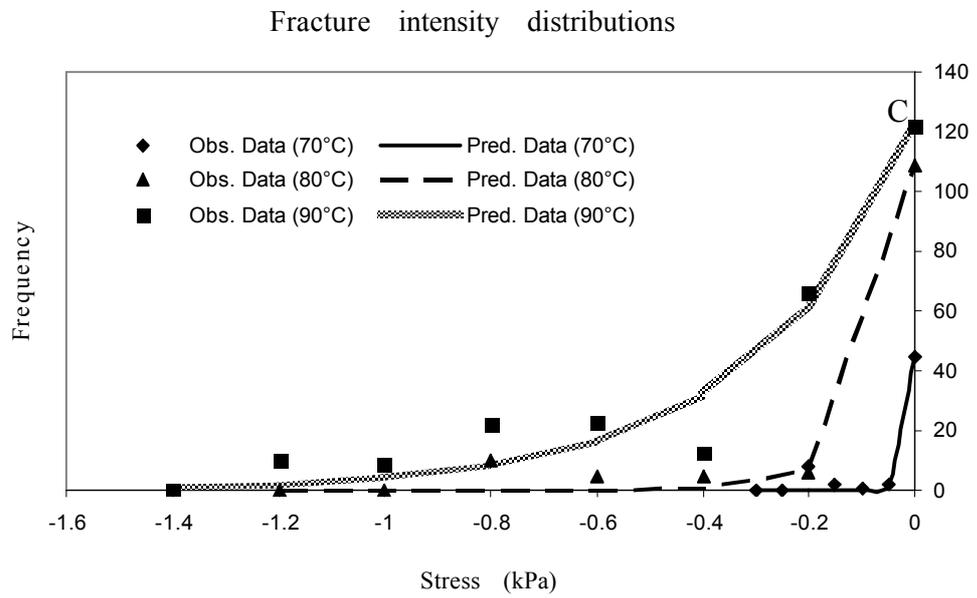
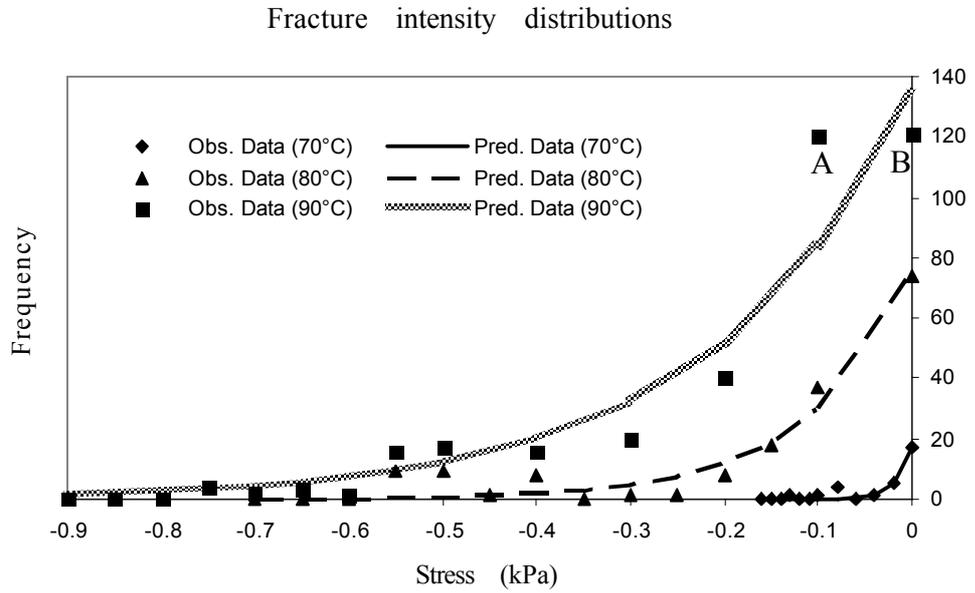


Figure 7

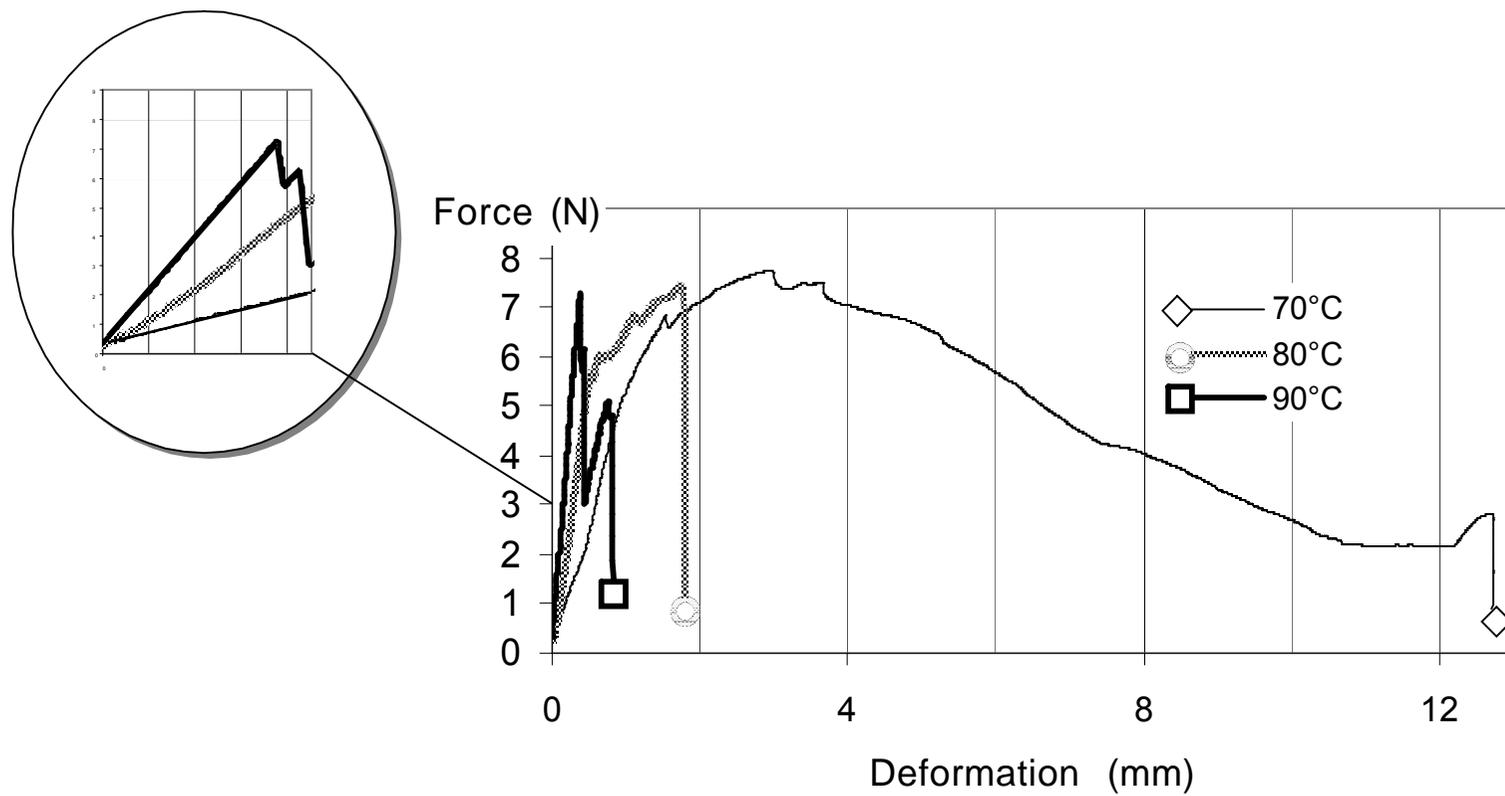
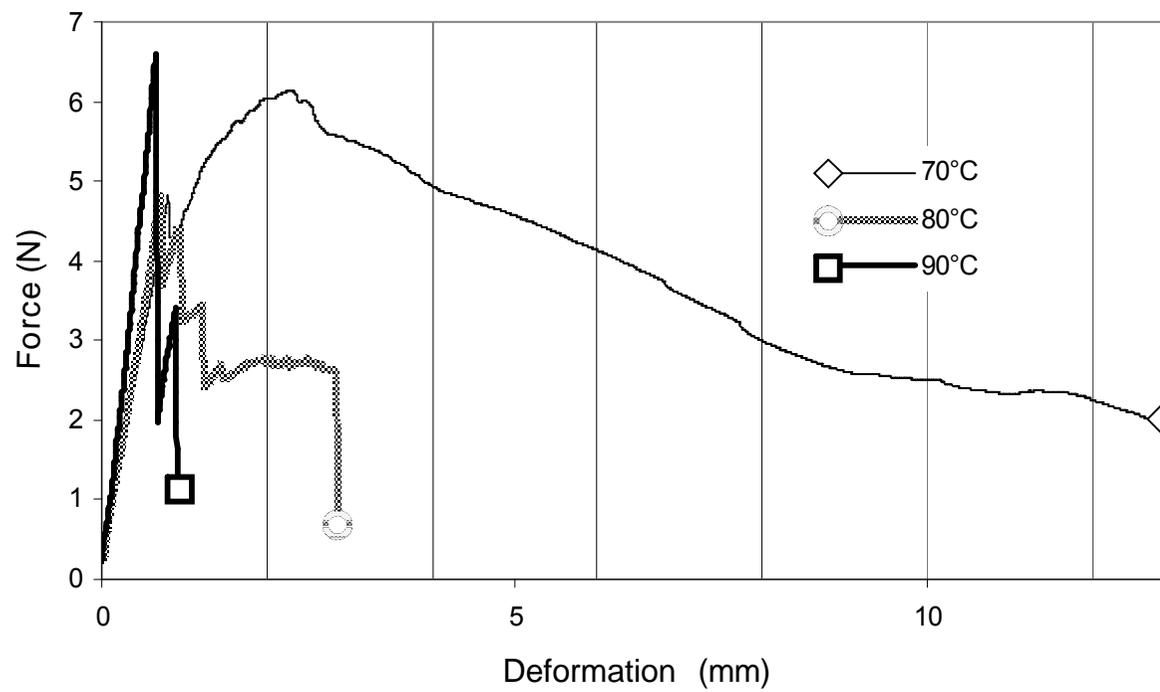


Figure 6



ANALYSIS / TEST TYPE	Pink Lady <sup>®</sup>			Golden		
	70°C	80°C	90°C	70°C	80°C	90°C
MOISTURE CONTENT (%)	3.541 <sup>a</sup> (±0.44)	2.064 <sup>b</sup> (±0.24)	1.548 <sup>c</sup> (±0.13)	4.282 <sup>d</sup> (±0.22)	2.671 <sup>e</sup> (±0.14)	1.845 <sup>f</sup> (±0.11)
WATER ACTIVITY	0.280 <sup>g</sup> (±0.0209)	0.240 <sup>h</sup> (±0.0157)	0.186 <sup>i</sup> (±0.0251)	0.263 <sup>g</sup> (±0.0242)	0.197 <sup>h</sup> (±0.0246)	0.155 <sup>i</sup> (±0.0108)
COMPRESSION- RELAXATION (mod.)						
$\sigma_r$	0.6875 <sup>j</sup> (±0.0065)	0.7885 <sup>k</sup> (±0.03)	0.8905 <sup>l</sup> (±0.0197)	0.6451 <sup>m</sup> (±0.0087)	0.7309 <sup>n</sup> (±0.0330)	0.8312 <sup>o</sup> (±0.0089)
$b$	61.288	14.003	3.328	60.711	9.279	4.724
$C$	16.665	40.363	44.841	6.283	27.917	49.952
$r^2$	0.967	0.983	0.946	0.937	0.948	0.916
$F_c$	58	135	265	29	166	360
$Pd$ $\geq 0.5\% F_{max}$	1.476 <sup>p</sup> (±0.32)	3.532 <sup>q</sup> (±0.40)	5.433 <sup>r</sup> (±0.22)	0.848 <sup>s</sup> (±0.16)	4.031 <sup>t</sup> (±0.54)	5.352 <sup>r</sup> (±0.28)
$Pd$ $\geq 5.0\% F_{max}$	0.508 <sup>u</sup> (±0.12)	1.825 <sup>p</sup> (±0.20)	4.046 <sup>t</sup> (±0.28)	0.321 <sup>u</sup> (±0.24)	1.665 <sup>p</sup> (±0.34)	3.517 <sup>q</sup> (±0.14)
BENDING-SNAPPING						
$E$ (kNmm <sup>-2</sup> )	1.904 <sup>v</sup> (±0.48)	3.081 <sup>w</sup> (±0.58)	4.683 <sup>x</sup> (±0.83)	0.961 <sup>y</sup> (±0.27)	1.990 <sup>t</sup> (±0.22)	2.553 <sup>q</sup> (±0.35)

Standard deviations are reported in brackets. Different letters denote statistically significant differences ( $p \leq 0.05$ )