

**Development of a tomato pomace biorefinery based on a CO<sub>2</sub>-supercritical extraction process for the production of a high value lycopene product, bioenergy and digestate.**

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**Abstract:** Tomato peels and seeds (TP) are the most abundant canning industry waste actually used to produce biogas. TP is rich in lycopene (lyc) and represent a more sustainable feedstock than tomato fruits actually employed. It was therefore chosen as feedstock together with supercritical CO<sub>2</sub> extraction (SFE-CO<sub>2</sub>) technology to develop a TP-SFE-CO<sub>2</sub> biorefinery, topic scarcely investigated. Two TP were tested and although TP-SFE-CO<sub>2</sub> parameters were the same, lyc recoveries depended by peel structure changes occurred during pre -SFE-CO<sub>2</sub> drying step. Higher moisture (102.7 g kg<sup>-1</sup> wet weight) permitted 97 % lyc recovery and gave a water-in-oil emulsion as extract. Mass balance confirmed that lyc isomerisation did not cause lyc losses. After a significant oil extraction, exhaust TP showed a biodegradability 64% higher than the raw one, attributable to fibre structure disruption. The biorefinery proposed (SFE\_CO<sub>2</sub>+anaerobic digestion) determined positive economic revenue (+787.9 € t<sup>-1</sup>TP) on the contrary of the actual TP management.

**Keywords:** lycopene, tomato pomace, anaerobic digestion, supercritical extraction, biorefinery

**Abbreviations:** tomato pomace (TP), lycopene (lyc), supercritical CO<sub>2</sub> extraction (SFE-CO<sub>2</sub>), tomato pomace named S (S<sub>raw</sub>), tomato pomace named A (A<sub>raw</sub>), intermediate moisture (IM), biogas potential production test (ABP), S<sub>raw</sub> exhaust fraction after TP-SFE-CO<sub>2</sub> (S<sub>exh</sub>), A<sub>raw</sub> exhaust fraction after TP-SFE-CO<sub>2</sub> (A<sub>exh</sub>), broken and intact cell (BIC).

## 1. Introduction

The tomato industry is one of the most developed for vegetable processing at both European and world level (World Processing tomato council, 2016) and is responsible for the production of huge amounts of waste that creates a major disposal problem for the industry in terms of costs and environmental impacts (Urbonaviciene and Viskelis, 2017). Tomato peels and seeds (i.e. tomato pomace - TP) are the most abundant solid waste fraction, representing 2-3% of the starting weight of tomatoes. TP was usually composted but more recently started to be used as feedstock for anaerobic digestion (AD). AD is a biological process that took advantage by microbial activity to produce biogas, a renewable fuel, which consists of CH<sub>4</sub> (50 - 80 volume volume<sup>-1</sup>) and CO<sub>2</sub> (Tani et al., 2006). Biogas production sector is currently on of the most sustainable energy production system and plays a key role in achieving the ambitious targets approved by the renewable EU energy directive (European Biogas Association, 2019). AD produces the digestate too, a solid stabilized biomass recognized as bio-based fertiliser by the new EU Fertiliser Regulation to replace synthetic N and P ones (Tambone et al., 2010; Riva et al., 2016; European Biogas Association, 2019).

High biodegradability is the most important biomass property to achieve high methane production. However, TP's homogenous composition and abundant bioactive components content imply that TP is the ideal biomass for further extraction of the valuable bioactive molecules and that the treated TP is only later used for bioenergy production. This fact, known as cascading use, led to an awareness of the need to develop a TP-based biorefinery to increase the productivity and efficient use of waste and by-product saving natural resources and reducing the waste production (Zero-waste principle) (Scoma et al., 2016).

TP is particularly rich in lycopene (lyc), the most powerful antioxidant carotenoid widely required by the cosmetic, food and pharmaceutical industries (Zunik et al., 2012). Thanks to its ability to act as

a quencher of singlet molecular oxygen radicals, lyc is one of ten carotenoids which are mainly marketed, with an economic value globally estimated of 1.5 USD billion on 2017 and a compound annual growth rate 2017-2022 (CAGR) of 2.3% (BBC Research, 2018).

Lyc is currently produced synthetically or extracted from tomato fruit cultivated for this purpose. Although the natural origin is a valuable market characteristic, actual production from fruits is no longer sustainable because of the agronomic cost, land consumption and food competition, so using TP represents an alternative source, making a transition from a first to a third generation production system (Urbonaviciene and Viskelis, 2017).

The lipophilic nature of lyc requires an apolar solvent such as ethylacetate to be extracted, which could leave traces affecting human health, especially when consumed daily (Zunik et al., 2012); in addition, the solvent evaporation step and final safe disposal increase the production costs (Nobre et al., 2009; Ollanketo et al., 2012; Kehili et al., 2017).

Already applied within the food industry, CO<sub>2</sub> supercritical technology (SFE-CO<sub>2</sub>) is an alternative extraction method that avoids the solvent organic employment to develop greener manufacturers and healthier extract solvent free (Zunik et al., 2012; Attard et al.; 2015; Kehili et al., 2017), in which TP seed oil acts as CO<sub>2</sub> co-solvent and becomes the lyc solubilisation medium. Lyc health benefits are improved during SFE-CO<sub>2</sub> since the trans form is partially transformed into cis, that has higher oil solubility and bioavailability (Müller et al., 2011; Richelle et al., 2012).

With the aim to achieve maximum yield, several SFE-CO<sub>2</sub> extraction configurations have been tested and the lyc recovery evaluated, using as reference feedstock content (Ollanketo et al.; 2001; Topal et al., 2006) since TP-SFE-CO<sub>2</sub> was usually developed as a single-purpose process however this approach gave a partial understanding of the phenomena occurred under supercritical conditions such as extract losses, chemical conversion or degradation (Scoma et al., 2016).

Developing a complete biorefinery aims to maximise productions applying a series of processes by using the exhaust fraction as feedstock. To our knowledge, only two scientific papers have explored this possibility (Kehili et al., 2016; Allison et al., 2017) for TP and encouraging results were obtained when SFE-CO<sub>2</sub> was the first production step since the exhaust fraction is solvent-free and dried, therefore easily employable.

In this perspective, the quali-quantitative characterisation of the exhaust biomass becomes a fundamental aspect to drive the next production step and the mass balance approach is an indispensable instrument to verify process performance. By accounting for in-and-out biomass amount and composition it was possible to calculate theoretical extract characteristics (amount and chemical composition) that could be compared with experimental data to reach better understanding of the SFE-CO<sub>2</sub> effect.

The aim of this work was to develop a TP-SFE-CO<sub>2</sub> based biorefinery to produce TP extract rich in lyc, while the second step was AD to produce biogas and digestate. The SFE-CO<sub>2</sub> extraction was described through a complete TP-SFE-CO<sub>2</sub> mass balance approach never developed before, and the exhaust TP was characterised to evaluate the feasibility of using it for biogas and digestate production achieving a zero-waste approach.

## **2. Experimental Section**

### *2.1 Materials*

Two different TPs derived by the industrial transformation of tomato for industry cultivars named respectively  $S_{\text{raw}}$  and  $A_{\text{raw}}$  were collected from a full scale tomato canning plant located in northern Italy (OPOE facility in XII Morelli, Emilia Romagna Region, Italy) during activities performed from July

2017 to September 2017; about 30 kg of each biomass was brought to the laboratory for analytical characterisation.

## *2.2 Tomato pomace characterisation*

### *2.2.1 Chemical Characterisation*

Dry matter (d.m.) and fibre composition were determined as previously reported (Van Soest et al., 1991). Fibre analyses were performed for neutral detergent fiber (NDF), acid detergent fiber (ADF), and acid detergent lignin (ADL) to calculate the cell soluble (CS), cellulose (ADF - ADL) and hemicellulose (NDF - ADF) content (Van Soest et al., 1991).

The protein content was calculated based on the total Kjeldahl nitrogen (TKN) (The US Composting Council, 1997) multiplied by the coefficient 5.7 (Piyakina and Yunusov, 1995).

Before SFE-CO<sub>2</sub>, S<sub>raw</sub> and A<sub>raw</sub> were partially dried in an oven at 50°C until they reached intermediate moisture (IM) contents of 50 g kg<sup>-1</sup> wet weight (w.w.) and 100 g kg<sup>-1</sup> w.w. respectively and the samples, named S<sub>rawIM</sub> and A<sub>rawIM</sub> were subsequently ground to 1-2 mm size. About 4 g of samples of S<sub>rawIM</sub> and A<sub>rawIM</sub> were extracted with 100 ml of hexane for 8 hours by using Soxhlet apparatus to measure oil content, which was calculated as the difference between the dried TP weight before and after extraction and retained as the reference to calculate the oil recovered by TP-SFE-CO<sub>2</sub>. The Soxhlet extracts were used to carry out the subsequent lyc characterisation and TEAC test (see section 2.2.3). All the analyses were performed in duplicate. Statistical elaboration of this work were performed with the SPSS statistical software (version 20) (SPSS, Chicago, IL).

### *2.2.2 Lycopene quantification and characterisation*

Lyc quali-quantitative characterisation was performed on an HPLC system (Agilent 1260 Infinity) equipped with a G1314F Agilent Uv/Vis spectrophotometer at 475 nm by using a C30 Develosil® rpaqueous column (5 µm, 250 x 4.6 mm). Hexane solution was injected at 25°C into the HPLC using as a mobile phase a mixture of methyl-tert-butyl ether (306975, Sigma Aldrich, USA) (solvent A) and a solution of methanol + triethanolamine 0.1% (solvent B) (34860-M and 90278 respectively, Sigma Aldrich, USA) with a flow rate of 1.2 ml min<sup>-1</sup>. The composition of the mobile phase was 15% A/85% B as the analysis began, to reach 55% A/45% B after 60 min and a final composition of 95% A/5% B after 65 min. All cis lyc isomer identification was based on the literature (Breitenbach et al., 2001; Urbonaviciene and Viskelis, 2017) and quantification was based on the trans-lyc analytical standard (L9879, Sigma Aldrich, USA).

### *2.2.3 Antiradical power assessment*

The TP antiradical properties were assessed by performing the TEAC (Trolox Equivalent Antioxidant Capacity) assay by evaluating the 2,2-azinobis-3-ethyl-benzothiazoline-6-sulfonic acid (ABTS<sup>+</sup>) radical cation decoloring reaction. ABTS<sup>+</sup> solution was prepared by mixing an ABTS<sup>+</sup> aqueous solution (7 mM) with potassium persulfate (2.45 mM, final concentration) and letting the mixture react in the dark at room temperature for 12–16 h. One hundred µl of extract was dissolved in 3.9 ml ABTS<sup>+</sup> solution, and 1 ml of the resulting solution was incubated for six minutes in the dark and then the solution absorbance was detected at λ=734 nm with a UV/visible Varian Cary 60 Spectrometer. Moreover, Trolox solutions (238813, Sigma Aldrich, USA) at different concentrations were used as standard. All the analyses were performed in duplicate.

### *2.2.4 Microscopic characterisation*

$S_{rawIM}$  and  $A_{rawIM}$  structures were investigated by scanning electron microscopy (SEM) and by optical microscopy. For SEM (Zeiss LEO 1430, Oberkochen, Germany) samples were gold-sputtered before observation at electron voltage of 5 kV, while thin TP sections (1 $\mu$ m thick) were stained with Toluidine Blue 1% in water and observed with a light microscope, Olympus BX-50 (Tokyo, Japan).

Cell wall ultrastructure was assessed using a transmission electron microscope (TEM) (Philips E208 transmission electron microscope, Philips Technology, Aachen, Germany). Samples were fixed in glutaraldehyde (2.5% v v<sup>-1</sup> in 0.1 M sodium cacodylate buffer pH 7.2) (Agar Scientific, Stansted, UK) for 2 h at 4°C, then washed with 0.1 M sodium cacodylate buffer for 1 h and post-fixed in osmium tetroxide (EMS, Hatfield, USA) (1% in water, w v<sup>-1</sup>) for 2 h. Samples were dehydrated in a series of ethanol solutions as described by D’Incecco et al. (2018), then embedded in Spurr resin (EMS, Hatfield, USA), and finally cured at 60°C for 24 h. Ultrathin (50–60 nm thick) sections were cut and stained with uranyl acetate and lead citrate (EMS, Hatfield, USA), both 0.2% in water (w v<sup>-1</sup>).

### *2.2.5 Biological Characterisation*

The biogas potential production test (ABP) was performed according to Scaglia et al. (2018). In brief, a 0.62 g d.m. sample, 37.5 ml of inoculum coming from digestate, and 22 ml of deionized water were put in 100-ml serum bottles. Digestate (d.m.= 34 g kg<sup>-1</sup> w. w., Volatile Solid- VS= 740 g kg<sup>-1</sup> d.m.) came from a full scale AD plant of North Italy; preliminary chemical characterisation (pH=8.33; Volatile Fatty Acids-VFA = 545 mg CH<sub>3</sub>COOH l<sup>-1</sup>; Total Alkalinity-TA= 1750 mg CaCO<sub>3</sub> l<sup>-1</sup>; VFA/TA= 0.31; Ammonia= 1460 mg l<sup>-1</sup>) confirmed the stable methanigen condition required to be employed as ABP test inoculum. The bottles were incubated at 37  $\pm$  1 °C for 90 days. The biogas production was determined periodically and expressed as NI kg<sup>-1</sup> d.m. In addition to the samples, inoculum and glucose ABP tests were done and employed as blank and positive control respectively. Samples ABP



production were thus calculated as: cumulative ABP less blank ABP ( $ABP=26 \text{ NI kg}^{-1} \text{ d.m.}$ ). All the analyses were performed in duplicate.

### *2.3 Tomato pomace supercritical CO<sub>2</sub> extraction process*

The  $S_{\text{rawIM}}$  and  $A_{\text{rawIM}}$  (1 kg wet weight, w.w.) were extracted in a pilot supercritical CO<sub>2</sub> extraction plant- SFE-CO<sub>2</sub> provided by Separeco S.r.l., Pinerolo (TO) Italy. The semi-industrial plant used was equipped with a 4.2 l extraction vessel, a 20 kWatt pump with a maximum flow rate of  $90 \text{ kg CO}_2 \text{ h}^{-1}$ , and 3 separators (gravimetric, heated cyclonic, cooled cyclonic). CO<sub>2</sub> flow was monitored with a Coriolis mass flow meter.

Extracting conditions were set as follows: pressure 38 Mpa, temperature  $80 \pm 1^\circ\text{C}$  and solvent ratio of  $103 \pm 4 \text{ kg CO}_2 \text{ kg}^{-1} \text{ d.m.}$  The extractions were carried out until no further extract recovery occurred and the kinetics monitored at 10, 20, 30, 60, 100  $\text{kg CO}_2 \text{ kg}^{-1} \text{ w.w.}$   $S_{\text{rawIM}}$  and 15, 30, 45, 65, 90  $\text{kg CO}_2 \text{ kg}^{-1} \text{ w.w.}$   $A_{\text{rawIM}}$ . The SFE-CO<sub>2</sub> extracts were frozen for subsequent characterisation. The TP-SFE-CO<sub>2</sub> exhaust fractions (named  $S_{\text{exh}}$  and  $A_{\text{exh}}$  for the  $S_{\text{rawIM}}$  and  $A_{\text{rawIM}}$  respectively) were weighed and chemically characterised as previously described, to perform the TP-SFE-CO<sub>2</sub> mass balance.

### *2.4 TP-SFE-CO<sub>2</sub> extract microscopic characterisation*

Extract composition was investigated using a LEICA DM R optical microscope. Sample drops were positioned on a microscope slide and observed without a cover glass under bright field (Perrechil et al., 2014). The emulsion was diluted with mineral oil and the images were acquired with a Leica EC3 camera and LAS V4.1 software.

In addition, emulsion microstructure was studied by using an inverted confocal laser scanning microscope (CLSM, Nikon A1<sup>+</sup>, Minato, Japan). The specimen was stained with Nile Red to detect

neutral lipids. A stock solution ( $1 \text{ mg ml}^{-1}$ ) was prepared in  $80\% \text{ v v}^{-1}$  DMSO (Sigma-Aldrich, St Louis, USA) and kept protected from light until use. Staining was performed at a concentration of  $100 \text{ }\mu\text{g ml}^{-1}$  and Nile Red was excited at 488 nm using an argon laser with the emission filter set at 520–590 nm. Separately, the staining with N-(lissamine rhodamine B sulfonyl) dioleoylphosphatidyl ethanolamine (Rh-DOPE), (Sigma–Aldrich, St. Louis, MO, USA and Avanti Polar Lipids Inc., Birmingham, England, respectively) was used to label phospholipids. A volume of  $40 \text{ }\mu\text{L}$  of Rh-DOPE solution ( $1 \text{ mg ml}^{-1}$  in chloroform) was placed in a glass vial and the chloroform was evaporated under nitrogen to avoid possible artefacts caused by this organic solvent. Then 1 ml of extract was added in the vial and kept at room temperature for at least 1 h prior to observation by CLSM. Rh-DOPE was excited at 543 nm wavelength and emission detected between 565 nm and 615 nm. Observations were performed using a 63x (numerical aperture NA 1.4) oil immersion objective.

Image analysis was performed using Fiji (ImageJ software, Research Services Branch, USA) on maximum projection of CLSM z-stack images. Four images per sample were used and analyses were performed in duplicate. Microsoft Excel (Microsoft Corp., Redmond, WA) was used to calculate the size distribution of the water droplets in the extract.

### **3. Results and Discussion**

#### *3.1. Choice of TP-SFE-CO<sub>2</sub> extraction process parameters*

Several lyc SFE-CO<sub>2</sub> processes tested different experimental conditions (Table 1) making difficult to identify which are fundamental extraction parameters to guarantee high lyc recovery (Baysal et al., 2000; Rozzi et al., 2002; Gómez-Prieto et al., 2003; Sabio et al., 2003; Topal et al., 2006; Vàgi et al., 2007; Ciurla et al., 2009; Nobre et al., 2009; Saldaña et al., 2010; Zhang et al., 2011; Machmudah et al., 2012; Honda et al., 2017; Vallecilla-Yeppez and Ciftci, 2018; Hatami et al., 2019). Temperature and pressure are always reported for their effect on solvent density and solvent vs. matrix

interaction (Topal et al., 2006); although their averages were almost constant (temperature= $77.4\pm 13.7^{\circ}\text{C}$  and  $P=37.3\pm 7$  MPa), lyc recovery was more variable (lyc recovery= $69\pm 22\%$  TP lyc) therefore these data were not enough to define extraction conditions. Flow rate and extraction-time ( $\text{CO}_2$  flux= $11 \pm 25$  kg  $\text{CO}_2$   $\text{h}^{-1}$  and extraction time= $211\pm 103$  min) were excessively changeable to identify reference to improve lyc recoveries (lyc recovery= $73\pm 18\%$  TP lyc and  $72\pm 20\%$  TP lyc for flow rate and extraction-time respectively).

Very few papers reported on the solvent ratio data, that is, the cumulative quantity of solvent required to extract the biomass. The average of  $100\pm 26.3$  kg  $\text{CO}_2$   $\text{kg}^{-1}$  TP corresponded to a lyc recovery of  $80\pm 10\%$  TP lyc that was the highest found among all parameters (Table 1). This result suggested its importance to drive the TP-SFE- $\text{CO}_2$  performance, therefore this flow rate, together with corresponding temperature and pressure (average temperature= $82\pm 4^{\circ}\text{C}$  and average pressure= $36.8\pm 8.3$  MPa) were applied in this work as follows: temperature= $80^{\circ}\text{C}$ , pressure= $38$  MPa, solvent ratio= $103$  kg  $\text{CO}_2$   $\text{kg}^{-1}$  TP (Table 1).

### *3.2 TP-SFE- $\text{CO}_2$ lyc kinetic extraction and peel morphology affect extraction yield.*

The  $A_{\text{rawIM}}$  had a lyc content ten times more concentrated than the  $S_{\text{rawIM}}$  (Table 2). Lyc content in tomatoes varies in function of many factors like cultivated variety, agricultural practices adopted, ripeness stage and storage conditions, and has been reported to range from 2.5 to 670 mg  $100$  g $^{-1}$  w.w. (Mayeaux et al., 2006; Akbudak et al., 2009). In addition, extractability of lyc is strictly linked to the TP moisture that at higher value (i.e. that of  $\text{TP}_{\text{raw}}$ ) reduced lyc vs. solvent interaction while at lower content got vegetal tissue dehydration lowering permeability.  $A_{\text{raw}}$  and  $S_{\text{raw}}$  had very high moisture (Table 2) thus preliminary drying steps were needed to reach optimal intermediate moisture (IM) to perform SFE- $\text{CO}_2$ . During drying pre-treatment lyc content of  $S_{\text{raw}}$  and  $A_{\text{raw}}$  were

monitored resulting similar for TPs for the same moisture content therefore the difference reported in Table 2 was attributable only to the modification occurred during pre-treatment.

In the raw tomato, trans lyc was the only form found (Shi et al., 1999), which was partially isomerized during industrial tomato processing and dehydration steps to get six cis molecules (Shi et al., 1999) (Table 2). For the  $S_{\text{rawIM}}$  the 9,13-cis-lyc, and 5,9-cis-lyc had the highest content followed by 15-cis-lyc and 7-cis-lyc while the  $A_{\text{rawIM}}$  showed a higher cis-lyc molecule number than the  $S_{\text{rawIM}}$  and the 7-cis-lyc and 5,9-cis-lyc were the most abundant molecules. The TP-SFE-CO<sub>2</sub> was able to extract 3.97 mg lyc kg<sup>-1</sup> d.m.  $S_{\text{rawIM}}$  and 91.63 mg lyc kg<sup>-1</sup> d.m.  $A_{\text{rawIM}}$  that corresponded to 73 % lyc  $S_{\text{rawIM}}$  and 97 % lyc  $A_{\text{rawIM}}$ , values almost different but within the ranges cited in the literature (Fig. 1; Table 1).

The lyc kinetics showed a first linear phase and a flatter second step (Fig. 1) associated with the lyc solvent solubility and lyc diffusion from the deeper tissues (Sabio et al., 2003; Vàgi et al., 2007). The first and second phases took longer for  $A_{\text{rawIM}}$  than for  $S_{\text{rawIM}}$ , implying that  $A_{\text{rawIM}}$  had a higher easily extractable lyc fraction in comparison with  $S_{\text{rawIM}}$  (Fig. 1).

Since the SFE-CO<sub>2</sub> extraction parameters were the same, biomass properties were assumed to affect the kinetics of extraction. Although data are not available for TP, a reliable model named “broken and intact cell-BIC” has been developed for seed oil SFE-CO<sub>2</sub> extraction (Fiori et al., 2009).

Basing on microscopic investigation, BIC considers biomass particles made up by several cell layers where, if the outer ones were partially broken during milling pre-treatment, the solute extraction was faster in comparison with intact cells located in the same coat and, above all, with those located in deeper layers (Vàgi et al., 2007; Fiori et al., 2009).

To verify this aspect, the TP peel fraction structure was investigated (Fig. 2).  $S_{\text{rawIM}}$  and  $A_{\text{rawIM}}$  peel remains had two main faces that corresponded to the external tomato fruit surface covered by

cuticle and to the parenchymatous cells layer located between the peel and pulp, in which polygonal wall structures were detected (Fig. 2 A, B, C, D). The peel faces observed did not show significant dissimilarities to explain the extraction trends, probably because TP peel had a more complicated structure than that of seeds (Fig. 2). Below the cuticle, there were a single-cell thick epidermal and two-four cutinized cell layers followed by the parenchymatous face (Crookes and Grierson, 1983) (Fig. 2 E, F). In comparison with fresh peel,  $S_{\text{rawIM}}$  and  $A_{\text{rawIM}}$  had enlarged intracellular spaces, cytoplasm that had become separated and evident wall thickness expansion; in fresh tissue, lyc is observable as crystals in the chromoplasts but in  $S_{\text{rawIM}}$  and  $A_{\text{rawIM}}$  it was not recognizable as a consequence of cytoplasm alteration (Fig. 2 E, F).

In comparison with the  $A_{\text{rawIM}}$ , the  $S_{\text{rawIM}}$  showed actual larger layer spaces. In the parenchymatous cells more evident wall shape widening occurred, in contrast with other cells positioned towards the cuticle surface. Structural damage to the peel was attributable to the thermal dewatering pre-treatment and to the duration of the process, which took longer for  $S_{\text{rawIM}}$  to reach the lower moisture content, causing very important morphological alterations (Table 2).

Ultrathin cross-sections' images were in addition analysed to better understand the modification occurred with the drying step (Fig. 2 G, H). At raw condition, cell wall was composed by cellulose microfibrils embedded in a hydrated matrix (water content of 75-90% w.w. cell wall) of hemicelluloses and pectins (Butchosa et al., 2019). TP cellulose crystallinity index of 34% meant that 66% of microfibrils had amorphous structure thus available to form bounds with other cell wall components over extended surface due to their big sizes (average thickness=32.24 nm, diameter of >45% microfibrils= 20-30 nm). Cellulose-OH were weakly linked to the other polysaccharides while very strong bounds were done with water that accumulated between microfibrils (Hubbe and Rojas, 2008; Szymańska-Chargot et al., 2017; Butchosa et al., 2019).

Upon drying procedure, the matrix collapsed above microfibrils and structure cell wall appeared thicker and more electron dense at the increasing of the water loss. Morphological changes corresponded to functional properties modifications such as lower porosity and higher rigidity of the cell wall that reduced in-out exchange capability across wall (Hubbe and Rojas, 2008; Szymańska-Chargot et al., 2017; Butchosa et al., 2019).  $S_{\text{rawIM}}$  cell wall was more electron-dense and 2-3 times thicker than  $A_{\text{rawIM}}$ , alterations explainable to the stronger dehydration degree (Li et al., 2014) (Fig. 2 G, H); the morphological difference supported the fact that  $S_{\text{rawIM}}$  in comparison with  $A_{\text{rawIM}}$  had lower attitude to the lyc extraction for the higher cell wall resistance that limited solvent way-in and lyc way-out cells in agreement with the kinetics (Fig. 1) (Saini and Keum, 2018).

### *3.3 TP moisture effect on the TP-SFE-CO<sub>2</sub> lycopene extraction yield*

Some authors consider the TP water content to be an important parameter that influenced the lyc extraction and defined TP optimal moisture as between 46 g kg<sup>-1</sup> w.w. TP and 228 g kg<sup>-1</sup> w.w. TP (Ge et al., 2002; Shi et al., 2006; Zunich et al., 2012; Nobre et al., 2016). Due to the very high starting moisture, the TP dehydrating step was done until it reached “TP partially dried -TP<sub>IM</sub>” with two different moisture contents that corresponded to the optimal range between medium ( $A_{\text{rawIM}}$ ) and lowest ( $S_{\text{rawIM}}$ ) values (Table 2)

$A_{\text{rawIM}}$  gave very good lyc recovery confirming that the moisture level chosen gave the best TP-SFE-CO<sub>2</sub> performance. However, some authors described, for a TP moisture content similar to that of the  $S_{\text{rawIM}}$ , cell membrane lipid modification that makes it impermeable, reducing lyc recovery (Shi et al., 2006; Zunich et al., 2012; Nobre et al., 2016). Previous data highlighted how pre-treatment greatly modified the cell walls, contributing to affect lyc recovery; however, no data were reported about additional effects occurring during SFE-CO<sub>2</sub> extraction, during which water is converted to

steam that generates intracellular pressure able to achieve, as an extreme effect, cell wall rupture and tissue unravelling (Floros and Chinnam, 1998). With the aim of verifying this phenomenon, peel morphological changes occurring during TP-SFE-CO<sub>2</sub> were investigated (Figs. 2, 3). No significant modification was found for the S<sub>exh</sub> cuticle face, while A<sub>exh</sub> showed several scratches not present before (Fig. 2 A, B, Fig. 3 A, B). TP-SFE-CO<sub>2</sub> temperatures reduced waxy resistance and the hydrophobic nature of the waxes allowed them to avoid the steam, resulting in increased intracellular pressure and enhanced cuticle rupture (Li et al., 2014). Nevertheless process conditions were not the only cause of this effect, that occurred only for A<sub>rawIM</sub> probably due to the higher water content that in the steam state created enough intracellular pressure to scratch the outer layer.

Parenchymatous faces (Fig. 3 C, D) also showed evident tissue disorganization if compared with the starting biomass, which was attributable to the steam effect (Fig. 2 C, D, Fig. 3 C, D). A<sub>exh</sub> had several empty and broken cells with thin walls; on the contrary, S<sub>exh</sub> cells appeared almost full showing very large thick walls that occupied most of the face surface.

Cross section images confirmed SEM data (Fig. 3 E, F). Both peel structures appeared less dense than the corresponding TP<sub>rawIM</sub> with dissimilar cellular fullness intensity in agreement with lyc recoveries (Fig. 2 E, F). S<sub>exh</sub> had cell wider walls than S<sub>rawIM</sub> and showed a progressive thickness reduction from the parenchymatous towards the cuticle face; for the same biomass cell fullness was maximum for epidermal layer below the cuticle and decreased in the direction of the parenchymatous face, indicating a different extractability tendency of the layers. A<sub>exh</sub> layers' cells appeared differently, seeming almost empty and showing similar cell wall conformation and interlayer space dimensions, suggesting a similar extractability for all cell layers. This last difference can be supposed to depend on the A<sub>rawIM</sub> cuticle scratches that improved cell solvent accessibility and solute exiting from cells more proxy to the cuticle, improving lyc recovery.

### 3.4 TP-SFE-CO<sub>2</sub> effect on extract physical, chemical composition and antioxidant power

The extracts accounted to 63.6 g kg<sup>-1</sup> S<sub>rawIM</sub> and 110.8 g kg<sup>-1</sup> A<sub>rawIM</sub> that represented 67 g kg<sup>-1</sup> d.m. S<sub>rawIM</sub> and 123.5 g kg<sup>-1</sup> d.m. A<sub>rawIM</sub>. The TP<sub>rawIM</sub> and TP<sub>exh</sub> comparison gave indications about the fractions' nature (Table 2), that were composed of oil for TP<sub>rawIM</sub> and oil plus water for the A<sub>rawIM</sub> (Table 2) meaning that S<sub>extract</sub> and A<sub>extract</sub> have different physical compositions.

With the aim to check extract quantity and composition, theoretical whole oil and water amounts were calculated by accounting for in-and-out TP weight (A<sub>rawIM</sub>=S<sub>rawIM</sub>= 1000 mg and S<sub>exh</sub>= 936.4 g kg<sup>-1</sup> S<sub>rawIM</sub> and A<sub>exh</sub>=890 g kg<sup>-1</sup> A<sub>rawIM</sub>) and oil and water contents (Table 2, 3). Theoretical extracts amounts were of 103.2 g kg<sup>-1</sup> S<sub>rawIM</sub> and 112.8 g kg<sup>-1</sup> A<sub>rawIM</sub>, derived together by the water plus oil. Experimental and calculated data fitted very well for the A<sub>extract</sub> that was composed of water: oil in the proportion of 70 % : 30 % weight A<sub>extract</sub>. S<sub>extract</sub> was theoretically composed of water and oil (water : oil being 29 %: 71 % weight S<sub>extract</sub>) but the experimental amount measured was less than that calculated, for a quantity that corresponded to a water fraction probably retained in the SFE-CO<sub>2</sub> plant and in any case statistically negligible (Table 2).

Microscopic investigation confirmed that S<sub>extract</sub> was oil and A<sub>extract</sub> was oil in which there were water droplets (Fig. 3). The difference was probably due to the available water amount that was higher for A<sub>rawIM</sub> and was thus co-extracted with oil during TP-SFE-CO<sub>2</sub> (Shi et al., 2009). Based on the drop measurement (water droplet size in the range 0.7 µm - 38.90 µm, with a mean diameter of 2.89 ± 3.60 µm) (see Supplementary Material) A<sub>extract</sub> was classified like a water in oil emulsion (W/O) of which the steady state was guaranteed by emulsifier molecules identified as phospholipids forming a layer around the water droplets (Fig. 3).



Lyc content was of 63 mg kg<sup>-1</sup> and 833 mg kg<sup>-1</sup> for S\_extract and A\_extract respectively and had a different trans:cis ratios (Table 3) with higher cis content in comparison with TP<sub>rawIM</sub> lyc. This change is called isomerisation and is fairly frequent when trans lyc is kept at 70-100°C (Yi et al., 2009) (Table 1, 3). Cis isomers had amorphous structure and higher lipophilicity than trans, therefore were more bioavailable, improving the extracts' health beneficial properties (Shi et al., 2009). From a quantitative point of view previous works considered isomerisation a degradative event that increased molecules' instability until they determined lyc loss (Urbonaviciene and Viskelis, 2017; Mutsokoti et al., 2017). In this work, thanks to the mass balance approach, lyc losses were excluded since the whole of the lyc extracted was calculated (3.84 mg kg<sup>-1</sup> d.m. S<sub>rawIM</sub> and 93.7 mg kg<sup>-1</sup> d.m. A<sub>rawIM</sub>) in agreement with the experimental values (Fig. 1); the same approach allowed us to calculate that very similar trans lyc fractions (14% trans lyc and 21% trans lyc amounts for the S<sub>rawIM</sub> and A<sub>rawIM</sub> respectively) were isomerized (Shi et al., 2009). The results seem to confirm that the chemical reaction depends above all on the temperature adopted: nevertheless, those data combined with the different lyc recovery rates, that depended on biomass properties, gave extracts with lyc compositions which were very dissimilar (Table 3).

Besides lyc concentration, the extracts' most important property for subsequent employment in the cosmetic, nutraceutical and food sectors is antioxidant power. A\_extract TEAC was three times higher than S\_extract in agreement with its higher lyc concentration (Table 3) and were together comparable with other lipophilic tomato extracts and powerful antioxidant molecules such as tocopherol (Longo et al., 2012).

The extracts' antioxidant power depended on the TP<sub>rawIM</sub> content and on the extraction process that was carried out at high temperature to increase lyc recovery while destroying other thermolabile molecules, a process which might have decreased the antioxidant properties (Shi and Maguer, 2000; Vàgi et al., 2007; Egydio et al., 2010; Liu et al., 2011; Kehili et al., 2016; Mutsokoti et al., 2017).

Effectively  $TP_{rawIM}$  had a very different lyc content (Table 2) but similar TEAC attributable to the whole antioxidant content (i.e. other carotenoids, lipids, tocopherols) (Shi and Maguer; 2000); however at the end of the TP-SFE- $CO_2$  extraction, TEAC were lower than those of the starting TP and more strictly linked to lyc (Table 1). With the aim to quantify whether the process effectively affected the antioxidant properties, mass balance was applied. Expected TEAC were of  $60.9 \text{ mmol kg}^{-1} S_{\text{extract}}$  and  $63.9 \text{ mmol kg}^{-1} A_{\text{extract}}$  that are respectively 80 % and 57% lower than those experimentally measured (Table 2, 3), giving numerical evidence of the supercritical extraction's huge TEAC reduction; moreover the high effect on  $S_{rawIM}$  in comparison with the  $A_{rawIM}$  could be partially explained by its lower extractability.

### *3.5 TP-SFE- $CO_2$ effect on the fibre composition and biodegradability*

TP were composed above all by recalcitrant fibers (ADL) attributable to the lignin, cutine, suberine of the tomato seed coats (Taylor and Salenka, 2012) plus hemicellulose and cellulose from peel; then the remaining fraction was the more easily degradable component (CS) made up mainly of oil and protein from the seeds (Del Valle et al., 2006) (Table 2). Although highly recalcitrant fibres formed the larger part of the TP,  $TP_{rawIM}$  had medium-high ABP value comparable with other biomasses employed as AD plant feed (Schievano et al., 2009), thanks to the oil and protein fractions' high specific biogas production ( $ABP_{oil} = 950 \text{ NI kg}^{-1} \text{ d.m.}$  and  $ABP_{protein} = 570 \text{ NI kg}^{-1} \text{ d.m.}$ ) (Wilkie, 2008).

Except for the  $S_{rawIM}$  CS, that depended on the oil extraction yield, TP-SFE- $CO_2$  did not determine macromolecular compositional changes, therefore for  $TP_{\text{exh}}$  a significant ABP reduction was expected and calculable by using the oil extract and  $ABP_{oil}$  as follows:  $ABP_{TP_{\text{exh}}} = [(ABP_{oil} * \text{oil extract (g)}/1000]$  (Table 2). Experimental  $TP_{\text{exh}}$  ABP not only disagreed with theoretical data ( $ABP_{S_{\text{exh}}} = 234 \text{ NI kg}^{-1} \text{ d.m.}$  and  $ABP_{A_{\text{exh}}} = 220 \text{ NI kg}^{-1} \text{ d.m.}$ ) but were even higher than the  $TP_{rawIM}$  meaning that

despite the  $TP_{exh}$  recalcitrant fraction being more concentrated than in  $TP_{rawIM}$ , biomass biodegradability increased after TP-SFE- $CO_2$ . The vegetal structural damage occurred during TP-SFE- $CO_2$  can lead to higher fibre bioavailability that did not depend on macromolecular concentration but rather on the fibre organization (Carpita and McCann, 2000) (Fig. 2, 3).

A first attempt to get phenomenon quantification was tried by calculating the biogas specific fibre production ( $ABP_{fibre}$ ) before and after TP-SFE- $CO_2$  (Table 2). To do so, TPs were considered to be composed with a good approximation by fibre (ADL+hemicellulose+cellulose) + oil + protein. Knowing  $TP_{rawIM}$ ,  $TP_{exh}$ , oil and protein amounts and oil and protein specific ABP production,  $ABP_{fibre}$  were estimated as  $ABP_{TP_{rawIM} \text{ or } exh} - [(ABP_{oil} * oil_{rawIM \text{ or } exh} (g)/1000) + (ABP_{protein} * protein_{rawIM \text{ or } exh} (g)/1000)]$ . The  $ABP_{fibre}$  was equal to 267 NI  $kg^{-1}$  d.m. and 252 NI  $kg^{-1}$  d.m. for the  $S_{rawIM}$  and  $A_{rawIM}$  then values became 406 NI  $kg^{-1}$  d.m. and 365 NI  $kg^{-1}$  d.m. for the  $S_{exh}$  and  $A_{exh}$  respectively that corresponded to an average biodegradability increase of 64%. This result agreed with previous works that described an increase of fibre availability measured as sugars-free fraction (Kehili et al., 2016). Ionic liquid (IL) was already able to improve fibre biodegradability, however exhaust biomass was IL polluted and unusable as AD feedstock (Allison and Simmons, 2017). On the contrary, SFE- $CO_2$  gave exhaust biomass solvent-free, dried and sterilised, characteristics that improved  $TP_{exh}$  re-usability respect to the  $TP_{raw}$ .

### *3.6. Biorefinery mass balance and economic feasibility*

Experimental data of this work were used to define the best TP-SFE- $CO_2$  process to get the maximum extraction yield possible. Results highlighted how not only the SFE- $CO_2$  parameters but also biomass properties (i.e. moisture, vegetal tissue morphology) are fundamental to reach high lyc recovery.

The experimental conditions adopted for  $A_{raw}$  guaranteed a better recovery than those applied for  $S_{raw}$ ; they were therefore applied to the biorefinery design.

With the aim to evaluate the economic feasibility of the process, experimental data (Table 2, Table 3) were applied to a typical tomato processing plant located in Emilia Romagna (North Italy), one of the most productive areas dedicated to the tomato cannery industry.

The tomato cannery plant has as an input of 60,000 t  $y^{-1}$  of tomato, that produced 1,800 t w.w. TP after industrial transformation. Actually  $TP_{raw}$  are destined to a near AD plant to integrate the feedstock intake commonly made by maize silage, a dedicated energy crops-EC which employment (.) guaranteed high biogas production ( $ABP=250 \text{ Nm}^3 \text{ ton}^{-1} \text{ w.w.}$ ) but was scarcely sustainable for the cultivation environmental and economic costs (Schievano et al., 2015; Paudel et al., 2019; Hol-Nielsen et al., 2009).

Due to low ABP ( $ABP=73 \text{ Nm}^3 \text{ ton}^{-1} \text{ w.w.}$ ) respect to the maize silage ( $ABP \text{ pf } TP_{raw}=29\%$  of ABP silage maize) and the limited storability,  $TP_{raw}$  was not considered a valuable AD feedstock and tomato cannery paid 10 €  $\text{ton}^{-1} \text{ w.w.}$  TP transport to AD plant (transportation cost= $18 \cdot 10^6 \text{ € } y^{-1}$ ).

By introducing the TP-SFE<sub>CO<sub>2</sub></sub> step there will be the production of 50.684 kg  $y^{-1}$  extract that, considering a lyc concentration of 833 mg  $\text{kg}^{-1}$  extract, corresponds to 42.22 kg  $y^{-1}$  lyc.

The feasibility of the new biorefinery was estimated taking into consideration the cost of manufacturing (COM) and the final product value. The COM was calculated considering the fixed capital investment (FCI), cost of operational labour ( $C_{oi}$ ) and cost of utilities ( $C_{ut}$ ) by applying the equation  $COM=0.28 \cdot FCI+2.73 \cdot C_{oi}+1.23 \cdot C_{ut}$  (Attard et al., 2016; Cristóbal et al., 2018) (see SI).

The elaboration allowed the estimate of the energetic needs and of the expenses for the production (SI). The  $A_{\text{rawIM\_SFE\_CO}_2}$  has a COM of 1,148,360 €  $\text{y}^{-1}$  that corresponded to 21.28 €  $\text{kg}^{-1}$  extract in agreement with those found for other carotenoids extraction (Pereira and Meireles, 2010).

To guarantee a prompt biorefinery integration into the local production system, the possibility to destine the  $A_{\text{exh}}$  to AD processes was evaluated.  $A_{\text{exh}}$  had a ABP of 360  $\text{Nm}^3 \text{ton}^{-1}$  w.w. that was around 5 times higher respect to that of  $\text{TP}_{\text{raw}}$  and 1.44 times higher than that of maize silage. This change depended by the moisture reduction and biodegradability increase occurred during first biorefinery steps (dryng+SFE- $\text{CO}_2$ ) that transformed  $\text{TP}_{\text{raw}}$  into a profitable and more sustainable AD feedstock respect to EC (Hol-Nielsen et al., 2009). Although  $\text{TP}_{\text{exh}}$  had a substitution capability of 1.44  $\text{ton}^{-1}$  w.w. maize silage, its economic value was estimated equal of that of silage maize (40 Euro  $\text{t}^{-1}$  w.w. ton, AD plant North Italy Owner communication) that, considering the  $A_{\text{exh}}$  amount (359.72  $\text{t w.w. y}^{-1}$ ) gave to the tomato cannery plant a potential economical revenue of + 14389 €  $\text{y}^{-1}$ .

The use of the  $\text{TP}_{\text{exh}}$  gave a theoretical biogas production of 129,648  $\text{Nm}^3 \text{y}^{-1}$  that corresponded to 62,037  $\text{Nm}^3 \text{y}^{-1}$  of methane, electric power productivity of 244,493  $\text{Kwh y}^{-1}$  and digestate as by-product (Schievano et al., 2015). Digestate is a biological stabilized, mature and sanitized biomass that has optimal composition to produce fertilizers (Tambone et al., 2010; Riva et al., 2016). In this perspective the solid/liquid separation is a commune refining treatment already applied to obtain N and N:P fertilizer respectively employable in substitution to those chemically synthesized as well as encouraged by the new EU Fertilising Product Regulation (European Biogas Association, 2019).

The economical sustainability of the process is directly linked to the market price of the product. Lycopene showed very different market values that depend on the source, production systems, lycopene concentration and physical state (crystalline or oleoresin). The high cost difference depends on the origin (synthetic or natural) and on the fact that a natural extract contains several bioactive

molecules. From chemical synthesis or from tomato solvent extraction plus purification, lyc crystalline product are available at costs of 3,000 € kg<sup>-1</sup> lyc (BCC Research, 2018). A different kind of product are tomato oleoresin, in which in addition to the lyc, there is a vast array of bioactive compounds (*i.e.* carotenoids, vitamins and phytosterols) which price is 50 € kg<sup>-1</sup> extract characterized by a lyc concentration of 1% that means a price of 5,000 € kg<sup>-1</sup> lyc.

Previous data did not take into consideration the SFE-CO<sub>2</sub> production system since presently, at the best of our knowledge, this kind of product is not available on the market. Another aspect that complicate the lyc price from SFE\_CO<sub>2</sub> price estimation is the different isomers composition in respect to synthetic and solvent-extract products that influenced the bioavailability and the final healthiness effect. Synthetic and solvent extract lyc are trans isomers (trans > 90% total lyc) that was less bioavailable than cis form (Boileau and Boileau, 2002), thus lyc mixture isomers composition influences body adsorptive effect; for example for lyc mixture trans:cys of 95:5 and 55:45 a adsorption degree of about 60% and 99% respectively was reported (Unlu et al., 2007).

Basing on the previous consideration and the A\_extract lyc characteristics, in this work we consider reasonable giving a price of 50 € kg<sup>-1</sup> A\_extract that corresponded to that of the oleoresin already on the market. This choice came by the fact that the estimation of the real price is actually unpredictable but, using as reference caffeine, for which synthetic, standard and supercritical extraction products are available in the market (de Melo et al., 2014; Pharmacompass. Com, 2016; Sigma-Aldrich web site, 2019), a higher price than that used in this work is reasonable. Therefore taking into account the market price, the extract amount and the COM, the total net revenue for the biorefinery would be 2,552,186 € y<sup>-1</sup>, meaning a profit of 1,403,826 € y<sup>-1</sup> that corresponds + 1,418,229 € y<sup>-1</sup> (+787.9 € t<sup>-1</sup>TP) respect to the actual TP management system.

#### 4. Conclusion

The TP\_SFE\_CO<sub>2</sub> biorefinery was made by: TP pre-drying until to reach moisture of 100 g kg<sup>-1</sup> w.w. TP that resulted an optimal compromise to contain vegetal tissue alteration and at the same time favourite lyc recovery during SFE-CO<sub>2</sub>. The extract was an emulsion rich in lycopene with a favourable trans isomer: cis isomer proportion that was estimated to a have a value of 50 € kg<sup>-1</sup> extract. The SFE-CO<sub>2</sub> acts as efficacious system to increase fibre biodegradability (+64%) and improved the TP<sub>exh</sub> characteristics to become a valid substituent of the silage maize actually employed to make AD to obtain bioenergy and fertilizers For a North Italy tomato cannery, TP biorefinery built by SFE-CO<sub>2</sub>+AD gave an additional economic revenue improving the production system of + 787.9 € ton<sup>-1</sup> w.w. TP<sub>exh</sub> respect to the actual system -10 € ton<sup>-1</sup> w.w. TP<sub>raw</sub>.

Table 1 TP-SFE-CO<sub>2</sub> process parameter adopted in literature.

Feedstock tipology	Feedstock amount (g)	CO <sub>2</sub> flow (kg h <sup>-1</sup> )	Temperature (°C)	Pressure (MPa)	Extraction time (min)	Solvent ratio (kg CO <sub>2</sub> kg <sup>-1</sup> feedstock)	Co-solvent (% feedstock weight)	lyc recovery (%lyc feedstock)	reference
Tomato fruit without seeds	10	20.4	40	40	360	n.r.	5, canola oil	n.r.	Saldaña et al., 2010
Tomato skin and pulp	0.5	0.113	45-35	n.r.	30	1600	-	69	Gómez-Prieto et al., 2003
Tomato fruit	3000	8-20	60-70	40-45	480	n.r.	50, powder roasted hazelnut	70	Ciurla et al., 2009
Tomato pulp	3	24.6	50	50	480	n.r.	-	n.r.	Honda et al., 2017
	3	0.114	86	34.5	200	91	-	71	Rozzi et al., 2009 <sup>b</sup>
	40-50	0.792	80	30	n.r. <sup>a</sup>	130	-	80	Sabio et al., 2003 <sup>b</sup>
TP	1000	80	80	46	60	80	-	90	Vàgi et al., 2007 <sup>b</sup>
	1.5	0.354	60	30	300	n.r.	-	93	Nobre et al., 2009 <sup>b</sup>
	1	n.r.	60	40	n.r.	n.r.	-	33	Zhang et al.; 2011 <sup>b</sup>



	4	0.142	90	40	210	n.r.	-	56	Machmudah et al., 2012 <sup>b</sup>
	10	0.24	80	40	120	n.r.	-	60	Kehili et al., 2017 <sup>b</sup>
	53	4	55	30	120	n.r.	5, ethanol	54	Baysal et al., 2000 <sup>b</sup>
	n.r.	0.085	100	40	390	n.r.	-	n.r.	Topal et al., 2006 <sup>b</sup>
	12	22.26	80	50	220	n.r.	-	52	Hatami et al., 2019
	20 (peel:seed 50:50)	8	80	30	280	n.r.	-	100	Vallecilla-Yepey and Cftci, 2018
Average value of each extraction parameter		11.6±25	77.4±13.7	37.3±7	211.1±102.6	100.3±26.3			
Extraction condition adopted in this work			80±1	38		103±4			

<sup>a</sup> n.r. not reported

<sup>b</sup> data used to define better extraction condition (see the text).

Table 2. TP chemical and biological characterisation

		$S_{raw}$	$S_{exh}$	$A_{raw}$	$A_{exh}$
d.m.		$218 \pm 0.10^{a,b}$		$228 \pm 0.8$	
	$g\ kg^{-1}\ ww$		$970 \pm 28.8A$		$974 \pm 45A$
d.m. <sub>IM</sub> <sup>c</sup>		$941 \pm 15.9bA$		$897 \pm 32bB$	
Total lyc	$mg\ kg^{-1}\ d.m.$	$5.79 \pm 0.31bB^d$	$1.78 \pm 0.11A$	$105 \pm 0.9aB^d$	$1.01 \pm 0.2A$
All-trans lyc	% total lyc	54	100	67	100
Cis-sum lyc		46	0	33	0
9,13-cis-lyc	% cis-sum lyc	45	0	9	0
15-cis-lyc		9	0	10	0
13-cis-lyc		0	0	3	0
5,13-cis-lyc		0	0	12	0
7-cis-lyc		14	0	39	0
5,9-cis-lyc		32	0	27	0
TEAC		$mmol\ Trolox\ kg^{-1}\ d.m.$	$10.8 \pm 1.37$	$7.79 \pm 0.98$	$11.1 \pm 1.12$
CS		$375 \pm 1.2bA$	$340 \pm 1A$	$286 \pm 1.9aA$	$288 \pm 5.4A$
oil		$102 \pm 23bB$	$25.1 \pm 2A$	$67.4 \pm 13aB$	$30.7 \pm 10A$
protein <sup>e</sup>	$g\ kg^{-1}\ d.m.$	$129 \pm 11aA$	$129 \pm 8A$	$140 \pm 15bA$	$148 \pm 14A$
hemicellulose		$60.9 \pm 3.7aA$	$50 \pm 5.4A$	$75.6 \pm 7.7aA$	$74.2 \pm 1.7A$
cellulose		$146 \pm 4.1aA$	$150 \pm 2.5A$	$169 \pm 3.9bA$	$172 \pm 7.6A$
ADL		$418 \pm 1.95aA$	$460 \pm 8.8A$	$470 \pm 1.9bA$	$466 \pm 11.3A$
ABP	$NI\ kg^{-1}\ d.m.$	$337 \pm 3aA$	$365 \pm 2B$	$324 \pm 2bA$	$370 \pm 3B$

<sup>a</sup> data followed by the same capital letter in the same line for the same TP-SFE-CO<sub>2</sub> are not statistically different (ANOVA Bootstrap, p<0.05)

<sup>b</sup> data followed by the small letter in the same line are not statistically different (ANOVA Bootstrap, p<0.05)

<sup>c</sup> d.m.<sub>IM</sub>:  $S_{rawIM}$  and  $A_{rawIM}$  dry matter content reached after partial dehydration step done before SFE-CO<sub>2</sub>

<sup>d</sup> Total Lyc concentration determined for the  $S_{rawIM}$  and  $A_{rawIM}$

<sup>e</sup> protein content calculated from the NTK \*5.7 (Piyakina and Yunusov, 1995)

Table 3. TP-SFE-CO<sub>2</sub> extract characterisation

		S_extract	A_extract
Total lyc	mg kg <sup>-1</sup> extract	40±5	619±22
All-trans lyc	% total lyc	23	54
Cis-sum lyc		77	46
X di-cis-lyc		7	0
9,13'-cis-lyc		36	22
15-cis-lyc		41	37
13-cis-lyc	% cis-sum lyc	2	1
5,13-cis-lyc		4	3
9-cis-lyc		1	23
7-cis-lyc		0	2
5,9-cis-lyc		9	12
TEAC	mmol Trolox kg <sup>-1</sup> extract	9.62±0.1	27.3±0.59

Cis isomers composition

Caption Figure:

Fig. 1 TP-SFE-CO<sub>2</sub> lyc and extract kinetic trend.

Fig. 2 TP<sub>rawIM</sub> peel fraction microscopy images: SEM S<sub>rawIM</sub> (A), A<sub>rawIM</sub> (B) cuticle and S<sub>rawIM</sub> (C) and A<sub>rawIM</sub> (D) parenchimatous faces; S<sub>rawIM</sub> (E) and A<sub>rawIM</sub> (F) light microscopy cross-sections in which CW means cell wall; CW ultrastructural TEM micrographs details of (G) S<sub>rawIM</sub> and (H) A<sub>rawIM</sub> where the former showed an expanded CW adjacent to median lamella (ml); scale bars are 20 μm in length (A-D), 10 μm in length (E-F) and 500 nm (G-H).

Fig. 3 TP<sub>exh</sub> peel fraction microscopy images: SEM S<sub>exh</sub> (A) A<sub>exh</sub> (B) cuticle face in which scratch is (S) and SEM S<sub>exh</sub> (C) and A<sub>exh</sub> (D) parenchimatous faces; Light microscopy cross-sections S<sub>exh</sub> (E) and A<sub>exh</sub> (F); scale bars are 20 μm in length (A-D) and 10 μm in length (E-F).

Fig. 4 Light microscopy images of S<sub>extract</sub> (A) and A<sub>extract</sub> (B). S<sub>extract</sub> is yellow uniformly coloured oil with cellular debris and A<sub>extract</sub> is dark orange coloured oil with water droplets (W). Confocal microscopy images of the A<sub>extract</sub> after labelling of neutral lipid by Nile red (C) and phospholipids by Rh-DOPE (D). Black spots are water droplets (W) dispersed in the oil phase (red background). Detail of the phospholipid layer at the oil/water interface (arrow) is enlarged in the panel (E); bars are 10 μm in length.

Fig. 1

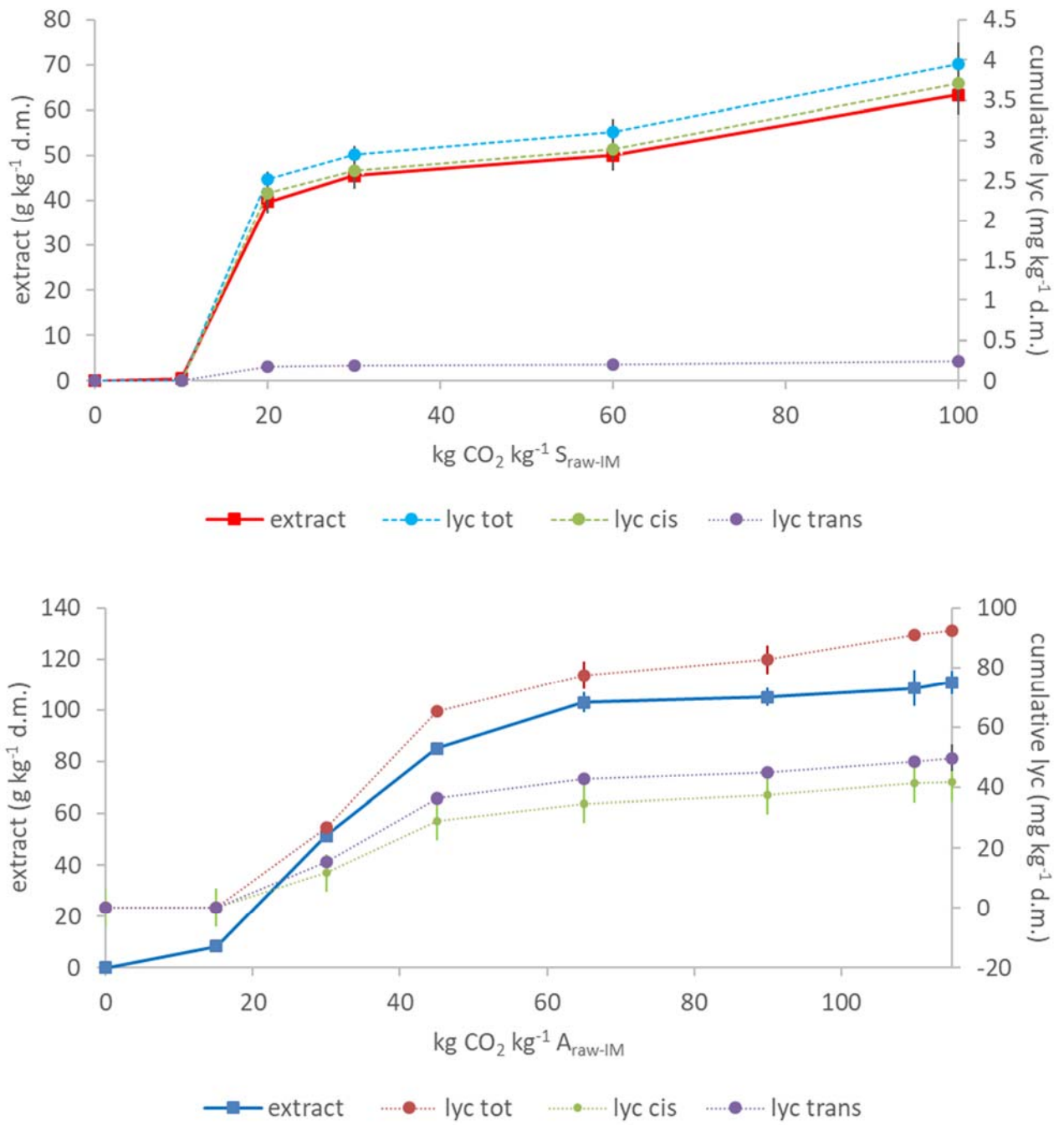


Fig. 2

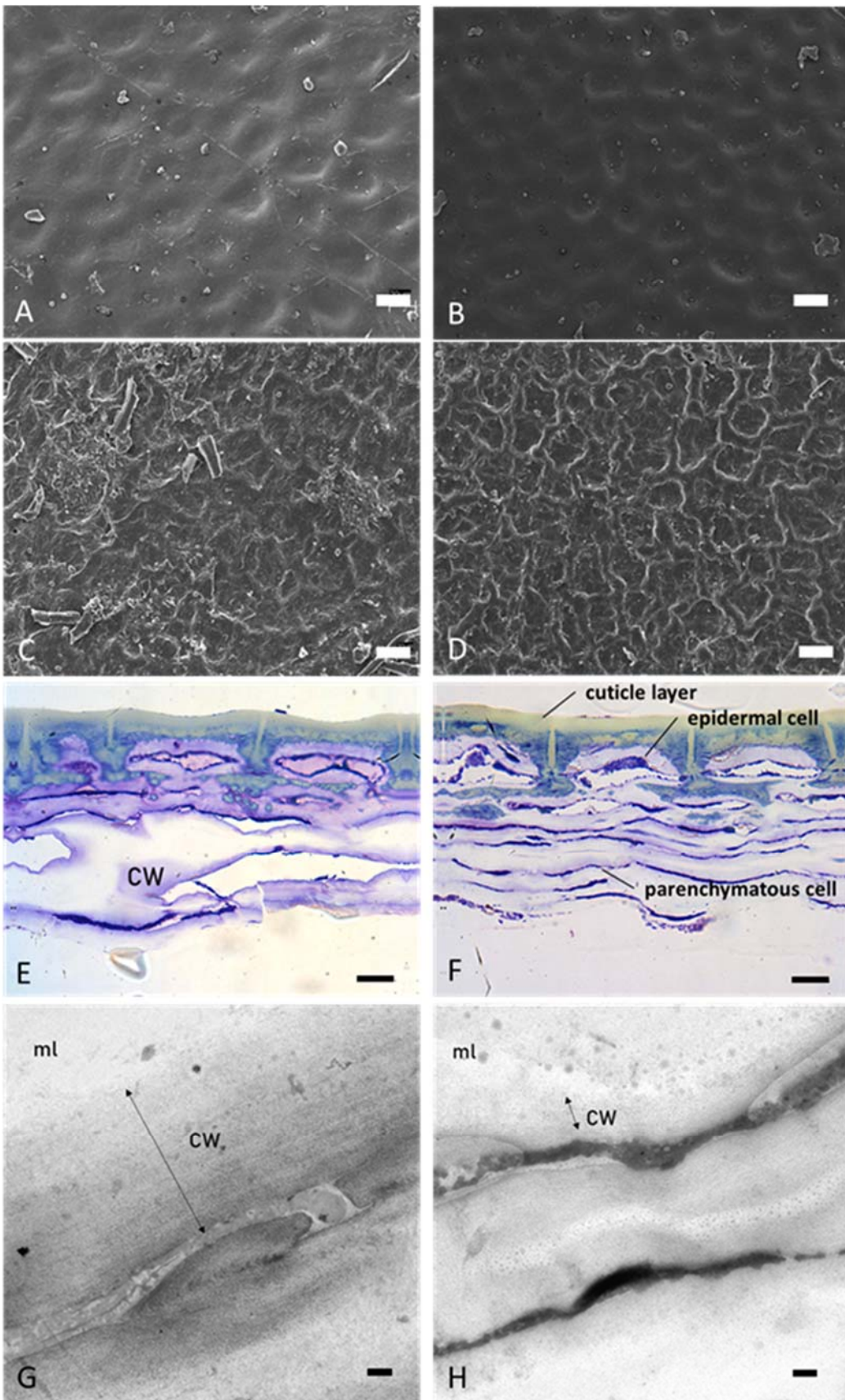


Fig. 3

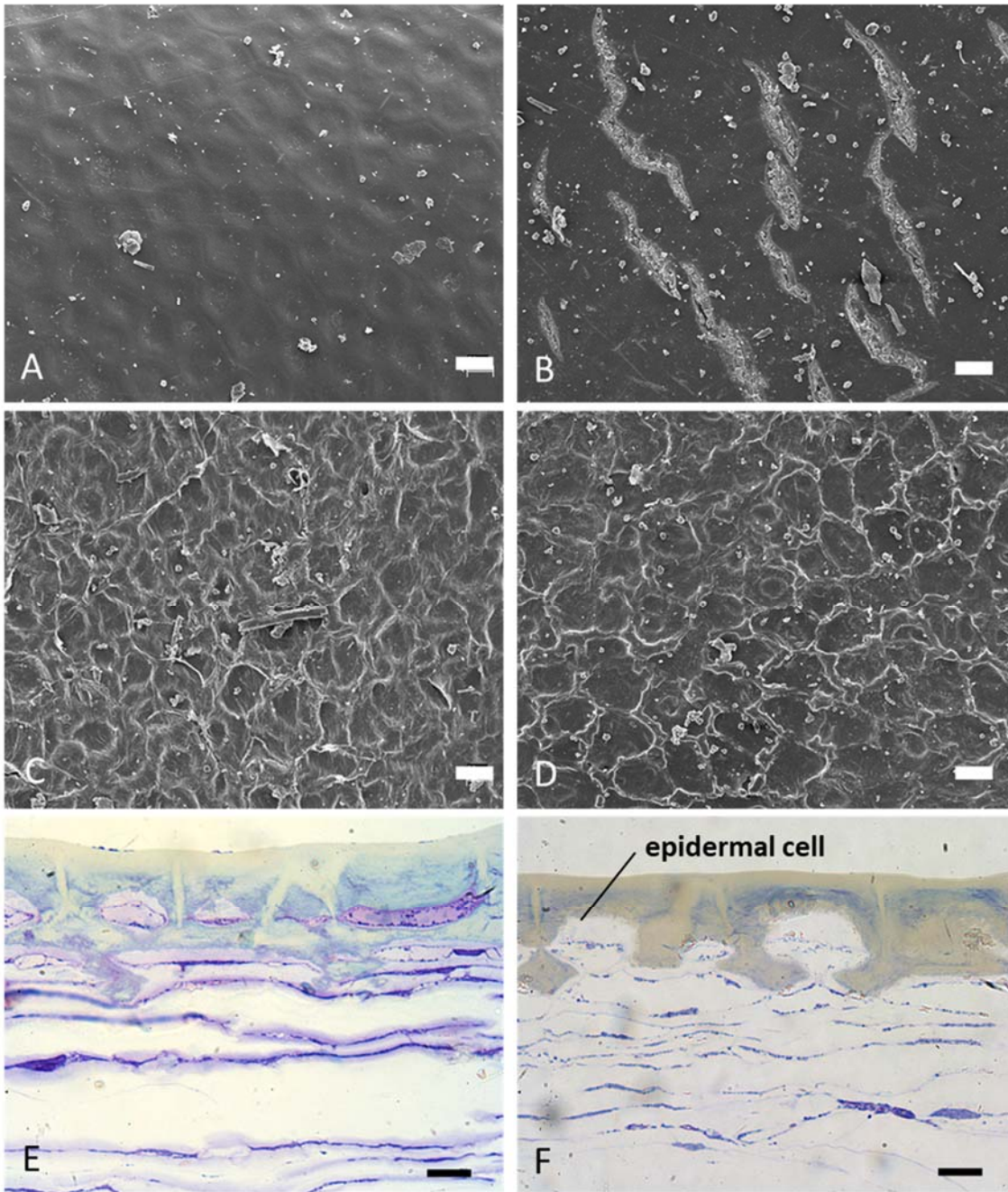
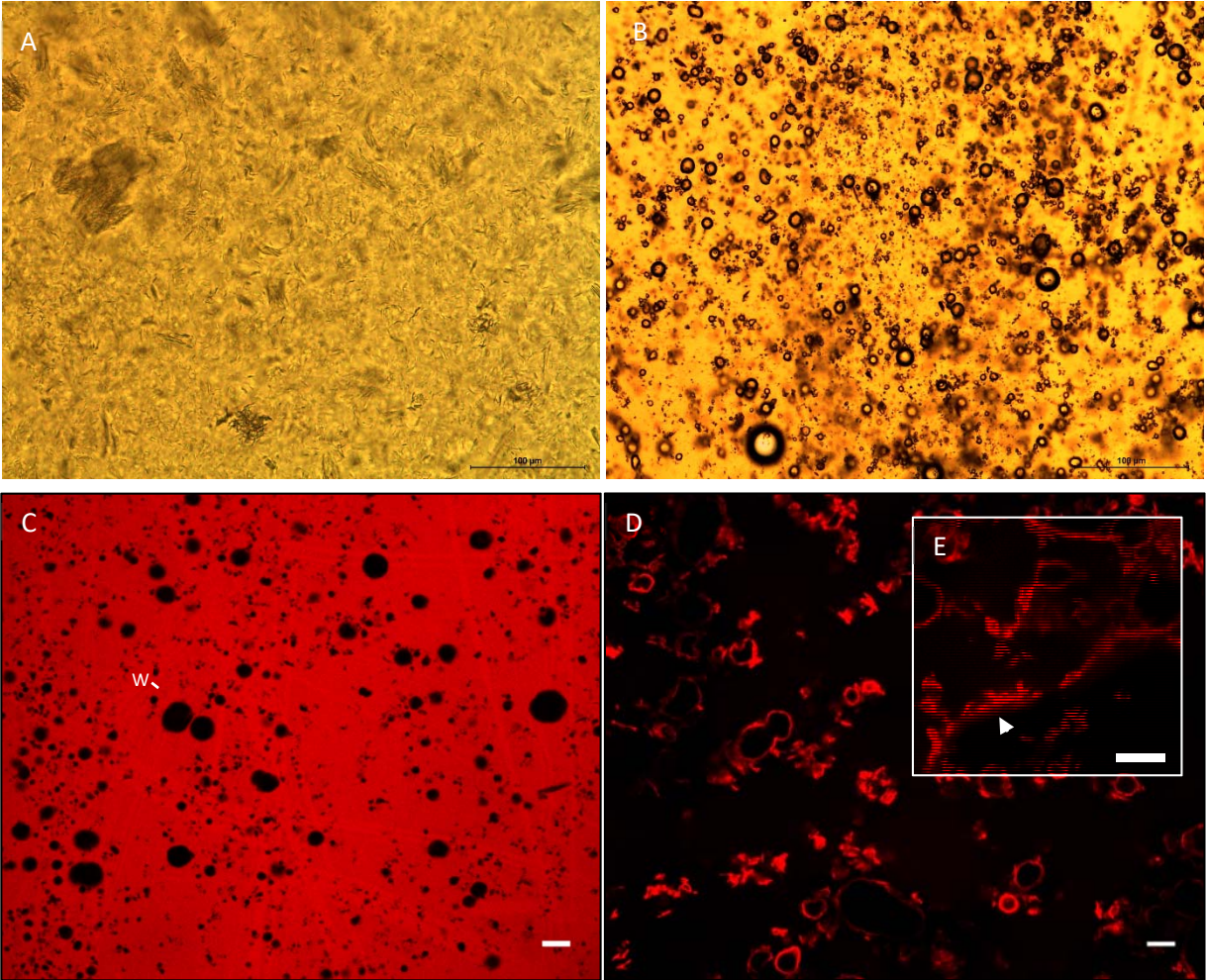


Fig. 4





**VISUAL ABSTRACT**

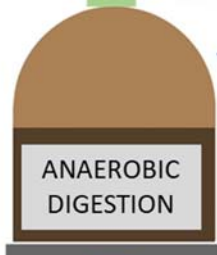
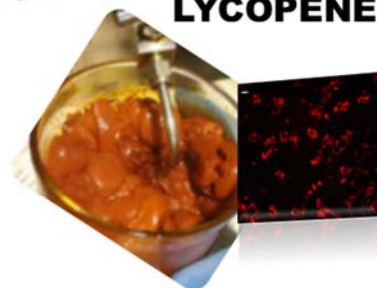
**TOMATO POMACE**



**EXHAUST TOMATO POMACE**



**EMULSION RICH IN LYCOPENE**



**BIOGAS**

**DIGESTATE**

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## Supporting Information

**Development of a tomato pomace biorefinery based on a CO<sub>2</sub>-supercritical extraction process for the production of a high value lycopene product, bioenergy and digestate.**

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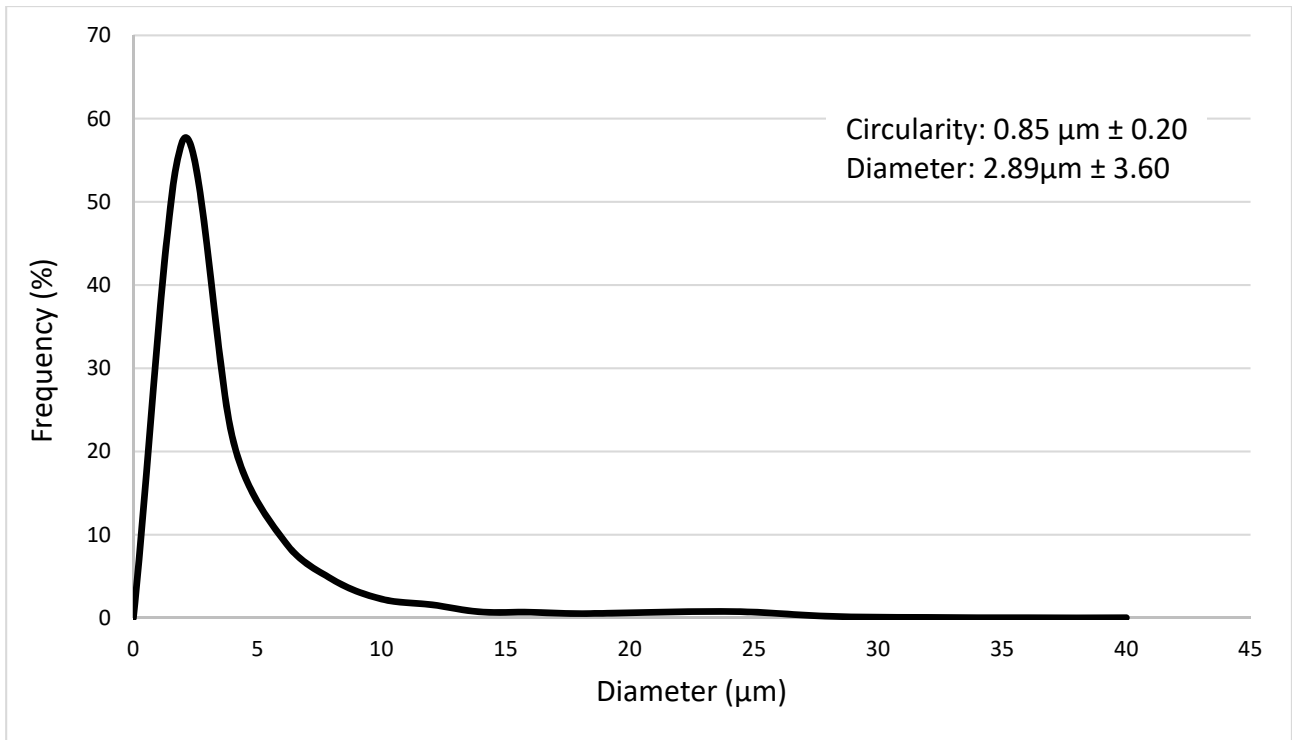


Fig. SI 1. Size distribution of water droplets obtained by image analysis of the CLSM images of the emulsion. Circularity and diameter of the water droplets are expressed as mean  $\pm$  standard deviation in the panel on the upper right side.



## **Cost of manufacturing (COM)**

To calculate the COM of an industrial process the main type of expenses to consider are the following:

1. Fixed capital investment (FCI): these are constant expenses mainly due to the cost of the apparatus required to carry out the process
2. Cost of operational labour ( $C_{ol}$ )
3. Cost of utilities ( $C_{ut}$ )
4. Cost of waste treatment: this parameter can be considered negligible since exhausted TP, the only waste resulting from the extractive process, will be employed to generate heat for the CO<sub>2</sub> heater.
5. Cost of raw material: this parameter can be considered negligible as well since TP is an industrial waste.

The total COM will be calculated with the equation  $COM=0.28*FCI+2.73*C_{ol}+1.23*C_{ut}$  (Cristobal et al., 2007).

## **Fixed capital investment**

The industrial supercritical extraction unit employed would be comprised of two 500 l extraction vessels, a CO<sub>2</sub> pump, a CO<sub>2</sub> heater, a refrigerator, and 3 separators (gravimetric, heated cyclonic, cooled cyclonic). The cost of the whole apparatus would be around 2000000 €. The fraction of investment can be calculated by multiplying the total investment by the depreciation rate, assumed to be 10 % per year. The cost of the CO<sub>2</sub> is negligible since the employed gas can be recirculated in the extraction unit.

### **Operational labour cost**

To determine  $C_{ol}$ , an hourly salary of 25 €  $h^{-1}$  is taken into account (EUROSTAT, 2017a). Considering that for every 6 h cycle an operator must be employed for 2 hours of labor (transporting the TP from the grinder, loading and unloading the extraction vessels), a total of 2640 h  $y^{-1}$  of work will be required. Hence, the total  $C_{ol}$  will be 66000 €  $y^{-1}$ .

### **Cost of utilities**

Five main parameters must be taken into account when estimating the costs of utilities: cost of electricity to dry the TP ( $C_{ut1}$ ), cost of electricity to grind the TP ( $C_{ut2}$ ) cost of the electricity used for the CO<sub>2</sub> pump ( $C_{ut3}$ ), costs associated with the CO<sub>2</sub> heater ( $C_{ut4}$ ), cost associated with the refrigerator ( $C_{ut5}$ ). The cost of electricity is considered 0.125 €  $kWh^{-1}$  (EUROSTAT, 2017b) and that of gas is 0.0083 €  $MJ^{-1}$  (EUROSTAT, 2017d). The flash drier employed consumed 14.5 kWh, while the grinder had an operating power of 5 kWh (Agrindustria Tecco, Cuneo). Considering that the two machines are modules of a single apparatus that can process up to 200 kg  $h^{-1}$  (up to a water content of 5 % w. w.  $^{-1}$  and a particle size of 0.2 mm), the whole 1800 t of TP can be processed with a total expenditure of 21900 €/y ( $C_{ut1} + C_{ut2}$ , 16300 and 5600 €  $y^{-1}$  respectively).  $C_{ut3}$  can be calculated when pressure, temperature, kg of CO<sub>2</sub> employed per kg of plant material and total dry TP are known: the extractor is operated at 380 bar and 80 °C, at which the specific enthalpy of CO<sub>2</sub> equals 343.16 kJ per kg of CO<sub>2</sub>, 103 kg of CO<sub>2</sub> per kg of plant material are used and 457 t of dry TP are processed yearly. Hence, the total  $C_{ut3}$  equals 561430 €  $y^{-1}$  ( $CO_2$ enthalpy\* $kg_{CO_2}$ \* $kg_{dry TP}$ ).

$C_{ut4}$  can be calculated by multiplying the heat required in MJ (Q) by the price of gas, following the equation  $Q=(M \cdot C_p \cdot \Delta T)/\text{efficiency}$ . M is the mass of CO<sub>2</sub> recirculated in the apparatus in a year (considering 4 cycles 4 h long per day, with a flow of 15 kg h<sup>-1</sup> and 330 working days per year), C<sub>p</sub> is the specific heat capacity of CO<sub>2</sub> at 80 °C (0.895 kJ kg<sup>-1</sup>) and ΔT is 76 °C, assuming an efficiency of 50 %, the yearly value of  $C_{ut4}$  will be 87000 €.

$C_{ut5}$  is calculated similarly, following the equation  $Q=M \cdot C_p \cdot \Delta T \cdot (\text{COP } 4^\circ\text{C})/(\text{COP } 20^\circ\text{C})$ . The fluid (water) required to refrigerate the apparatus has to be cooled from 20 to 4 °C, with a resulting Coefficient Of Performance (COP) of 0.08 and 0.15 respectively. The C<sub>p</sub> of CO<sub>2</sub> at 27 °C is 0.846 kJ kg<sup>-1</sup>.  $C_{ut5}$  is calculated similarly, following the equation  $Q=M \cdot C_p \cdot \Delta T \cdot (\text{COP } 4^\circ\text{C})/(\text{COP } 20^\circ\text{C})$ .;the fluid (water) required to refrigerate the apparatus has to be cooled from 20 to 4 °C, with a resulting Coefficient Of Performance (COP) of 0.08 and 0.15 respectively thus the C<sub>p</sub> of CO<sub>2</sub> at 27 °C is 0.846 kJ kg<sup>-1</sup> therefore the final value for  $C_{ut5}$  will be 71280 € y<sup>-1</sup>.

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